

文章编号: 1000-8152(2011)04-0575-06

## 时滞依赖网络控制系统的量化控制: 分段时滞法

褚红燕<sup>1,2</sup>, 费树岷<sup>2</sup>, 刘金良<sup>3</sup>, 翟军勇<sup>2</sup>

(1. 南京师范大学 能源与机械工程学院, 江苏南京 210042;

2. 东南大学 自动化学院, 江苏南京 210096; 3. 东华大学 信息科学与技术学院, 上海 201620)

**摘要:** 为了减小时滞依赖系统分析的保守性, 获得较大的时滞上界, 也为了减小网络中的数据传输率, 本文提出了一种具有量化的网络控制系统的新的分析方法: 时滞分段法。将时滞落于某一段小区间看做一种情形, 针对每种不同情形利用不同的自由权矩阵, 并利用矩阵函数的凸性, 得到了新的时滞依赖的稳定性条件。通过求解若干组线性矩阵不等式可得时滞上界和量化状态反馈控制器增益。仿真结果说明了本文所述方法的有效性。

**关键词:** 时滞依赖; 分段分析法; 矩阵函数凸性

**中图分类号:** TP273      **文献标识码:** A

## Quantized control for delay-dependent networked control systems: piecewise delay method

CHU Hong-yan<sup>1,2</sup>, FEI Shu-min<sup>2</sup>, LIU Jin-liang<sup>3</sup>, ZHAI Jun-yong<sup>2</sup>

(1. School of Energy and Mechanical Engineering, Nanjing Normal University, Nanjing Jiangsu 210042, China;

2. School of Automation, Southeast University, Nanjing Jiangsu 210096, China;

3. College of Information Science and Technology, Donghua University, Shanghai 201620, China)

**Abstract:** The piecewise delay method for quantized networked control system is proposed for reducing the conservativeness in the delay-dependent analysis, raising the delay upper bound and lowering the data transmission rate in the network. The delay-falling in one small subinterval is treated as a case. For different cases we adopt different free weighting matrix, and make use of the convexity of the matrix function to derive the corresponding stability criteria. The upper bound of the delay and the gain of the quantized state feedback controller can be determined by solving several sets of linear matrix inequalities. Numerical examples demonstrate the effectiveness of the proposed method.

**Key words:** delay-dependent; piecewise analysis method; convexity of the matrix function

### 1 引言(Introduction)

利用网络来传递控制信息的网络控制系统(NCS)受到广泛关注。Zhang等<sup>[1]</sup>研究了定常时滞NCS的稳定性, Yue等<sup>[2]</sup>首次建立了考虑网络时变时滞、丢包和错序的新的NCS模型, Peng等<sup>[3]</sup>研究了区间时变时滞NCS, 通过引入Jessen不等式降低了复杂性。Yue和Liu等首次采用时滞中点(DCP)法<sup>[4]</sup>来研究时滞系统<sup>[5,6]</sup>, 并进一步将时滞细分<sup>[7]</sup>, 得出了线性系统的保守性较小的稳定性条件。

上述针对系统的分析及设计都假设信号为无损传输, 然而, 在实际工业系统中, 这种假设通常不成立。比如, 在水下通讯控制系统中, 传输介质的有限传输能力对闭环系统的影响将变得不可忽略; 再比如NCS中各网络节点在地理上的分布越来越广, 彼此之间需要通过一个共享网络进行数据交换, 公共

网络的不可靠性导致网络阻塞现象时有发生, 因此其有限的传输能力必然会对在线控制产生巨大的影响, 因此数据量化处理在实际工业控制系统中是必要的。文献[8]针对量化控制系统模型, 在采用随机重复性试验测量信息的基础上, 提出了基于辅助模型的量化系统参数辨识方法。Tian等<sup>[9]</sup>研究了NCS的输出反馈量化控制, 放缩技术的使用带来了较大的保守性, Niu等<sup>[10]</sup>建立了具有量化和丢包的NCS的随机模型。文献[11]基于定常量化器研究了NCS的保成本控制, 但该量化控制不能保证其收敛到平衡点。

本文首先在传感器和控制器和控制器和执行器之间增加两个时变量化器, 建立了区间时变时滞的具有量化的NCS模型, 其次采用时滞分段法, 将时滞分成3段, 从而分3种情况对该系统进行稳定性分析和控制器设计。系统结构图如图1所示。

收稿日期: 2010-2-10; 收修改稿日期: 2010-5-31。

基金项目: 国家自然科学基金资助项目(60835001); 中国高等教育博士专项研究基金资助项目(20090092120027); 江苏省高校自然科学基金资助项目(10KJB510009)。

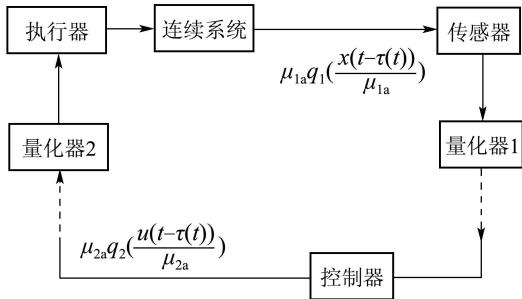


图 1 系统结构图

Fig. 1 Structure of the system

## 2 系统描述和引理(Description and lemmas)

**引理 1** 设  $\tau(t) \in [\tau_m, \tau_M]$ , 则对任意  $\Xi_1, \Xi_2, \Phi$ ,  
 $(\tau(t) - \tau_m)\Xi_1 + (\tau_M - \tau(t))\Xi_2 + \Phi < 0$

成立当且仅当如下不等式成立:

$$(\tau_M - \tau_m)\Xi_1 + \Phi < 0, (\tau_M - \tau_m)\Xi_2 + \Phi < 0.$$

### 2.1 时变量化器(Time-varying quantizers)

为了减小网络传输的数据量, 本文采用量化器  $\mu q(\mu^{-1}z)$ , 且满足如下不等式:

$$\begin{aligned} \| \mu q(\mu^{-1}z) - z \| &\leq \mu \Delta, \| z \| \leq \mu F, \\ \| \mu q(\mu^{-1}z) \| &> \mu(F - \Delta), \| z \| > \mu F, \end{aligned}$$

其中:  $F$  为量化范围,  $\Delta$  为量化误差,  $z$  和  $\mu$  的大小将会改变  $F$  和  $\Delta$ , 从而对于大信号加快量化速度, 而对于小信号增加量化精度.

### 2.2 系统描述(Description of the system)

如下线性网络控制系统:  $\dot{x}(t) = Ax(t) + Bu(t)$ , 其中  $x(t) \in \mathbb{R}^n$ ,  $u(t) \in \mathbb{R}^m$  分别为状态向量和控制输入向量,  $A$  和  $B$  为适当维数的时常矩阵. 考虑到网络时滞和量化的影响, 传递至控制器的状态量为

$$\bar{x}(t) = \mu_1 q_1(\mu_1^{-1}x(t - \tau(t))),$$

则控制器  $u(t) = \mu_2 q_2(\mu_2^{-1}K\mu_1 q_1(\mu_1^{-1}x(t - \tau(t))))$ , 其中  $\tau(t) \in [\tau_m, \tau_M]$ ,  $\tau_m, \tau_M$  为传输时滞的上下界. 则系统模型为:

$$\begin{cases} \dot{x}(t) = \\ Ax(t) + B\mu_2 q_2(\mu_2^{-1}K\mu_1 q_1(\mu_1^{-1}x(t - \tau(t)))) = \\ Ax(t) + BKx(t - \tau(t)) - B\mu_2 \delta(\mu_1, \mu_2), \\ x(t) = \Phi(t), t \in [\tau_M, 0], \end{cases} \quad (1)$$

其中

$$\begin{aligned} \delta(\mu_1, \mu_2) &= \\ \mu_2^{-1}Kx(t - \tau(t)) - q_2(\mu_2^{-1}K\mu_1 q_1(\mu_1^{-1}x(t - \tau(t)))) &. \end{aligned}$$

## 3 稳定性分析(Stability analysis)

**定理 1** 若存在矩阵  $P > 0$ ,  $T > 0$ ,  $Q_1 > 0$ ,

$R_i (i = 1, \dots, 4) > 0$  以及适当维数的矩阵  $M_j$ ,  $N_j (j = 1, 2, 3)$ , 使得下列线性矩阵不等式成立:

$$\begin{bmatrix} \Pi_k + T & \beta M_k \\ \beta M_k^T & -\beta R_{k+1} \end{bmatrix} < 0, \quad (2)$$

$$\begin{bmatrix} \Pi_k + T & \beta N_k \\ \beta N_k^T & -\beta R_{k+1} \end{bmatrix} < 0, \quad (3)$$

其中:

$$k = 1, 2, 3, \Pi_k = \Phi_k + \Xi_1^k + \Xi_1^{kT},$$

$$\Phi_1 = \begin{bmatrix} W_1 & * & * & * & * & * \\ R_1 & L_1 & * & * & * & * \\ 0 & 0 & 0 & * & * & * \\ 0 & 0 & 0 & -Q_3 - \frac{R_3}{\beta} & * & * \\ 0 & 0 & 0 & \frac{R_3}{\beta} & L_1 - \frac{R_4}{\beta} & * \\ 0 & 0 & 0 & 0 & \frac{R_4}{\beta} & -Q_4 - \frac{R_4}{\beta} \\ P & 0 & 0 & 0 & 0 & W_2 \end{bmatrix},$$

$$\Phi_2 = \begin{bmatrix} W_1 & * & * & * & * & * \\ R_1 & L_1 - \frac{R_2}{\beta} & * & * & * & * \\ 0 & 0 & 0 & * & * & * \\ 0 & \frac{R_2}{\beta} & 0 - Q_2 - \frac{R_2}{\beta} & * & * & * \\ 0 & 0 & 0 & 0 & L_2 & * \\ 0 & 0 & 0 & 0 & \frac{R_4}{\beta} - Q_4 - \frac{R_4}{\beta} & * \\ P & 0 & 0 & 0 & 0 & W_2 \end{bmatrix},$$

$$\Phi_3 = \begin{bmatrix} W_1 & * & * & * & * & * \\ R_1 & L_1 - \frac{R_2}{\beta} & * & * & * & * \\ 0 & 0 & 0 & * & * & * \\ 0 & \frac{R_2}{\beta} & 0 L_3 - \frac{R_3}{\beta} & * & * & * \\ 0 & 0 & 0 & \frac{R_3}{\beta} - Q_3 - \frac{R_3}{\beta} & * & * \\ 0 & 0 & 0 & 0 & -Q_4 & * \\ P & 0 & 0 & 0 & 0 & W_2 \end{bmatrix},$$

$$\Xi_1^1 = [-SA \ N_1 \ -SBK - N_1 + M_1 \ -M_1 \ 0 \ 0 \ S],$$

$$\Xi_1^2 = [-SA \ 0 \ -SBK - N_2 + M_2 \ N_2 \ -M_2 \ 0 \ S],$$

$$\Xi_1^3 = [-SA \ 0 \ -SBK - N_3 + M_3 \ 0 \ N_3 \ -M_3 \ S],$$

$$W_1 = Q_1 + Q_2 + Q_3 + Q_4 - R_1,$$

$$W_2 = \tau_m^2 R_1 + \beta R_2 + \beta R_3 + \beta R_4,$$

$$L_1 = -Q_1 - R_1, \quad L_2 = -Q_3 - \frac{R_4}{\beta}, \quad L_3 = -Q_2 - \frac{R_2}{\beta}.$$

且量化器满足如下条件:

$$2\Delta \| SB \| \| T^{-1} \| \leq \frac{\| x(t) \|}{\mu_2} \leq F_1,$$

$$F_2 \geq \|K\|(\Delta_1 + F_1),$$

则系统(1)渐近稳定.

**证** 设  $l = 3$ ,  $\beta = (\tau_m - \tau_m)/3$ ,  $\tau_1 = \tau_m + \beta$ ,  $\tau_2 = \tau_m + 2\beta$ , 构造如下Lyapunov函数:

$$\begin{aligned} V(x) = & x^T(t)Px(t) + \int_{t-\tau_m}^t x^T(s)Q_1x(s)ds + \\ & \int_{t-\tau_1}^t x^T(s)Q_2x(s)ds + \\ & \int_{t-\tau_2}^t x^T(s)Q_3x(s)ds + \\ & \int_{t-\tau_m}^t x^T(s)Q_4x(s)ds + \\ & \tau_m \int_{t-\tau_m}^t \int_s^t \dot{x}^T(v)R_1\dot{x}(v)dvds + \\ & \int_{t-\tau_1}^{t-\tau_m} \int_s^t \dot{x}^T(v)R_2\dot{x}(v)dvds + \\ & \int_{t-\tau_2}^{t-\tau_1} \int_s^t \dot{x}^T(v)R_3\dot{x}(v)dvds + \\ & \int_{t-\tau_m}^{t-\tau_2} \int_s^t \dot{x}^T(v)R_4\dot{x}(v)dvds, \end{aligned}$$

设

$$\xi^T(t) = [x^T(t) \ x^T(t-\tau_m) \ x^T(t-\tau(t)) \ x^T(t-\tau_1) \ x^T(t-\tau_2) \ x^T(t-\tau_m) \ \dot{x}^T(t)].$$

**情形1**  $\tau(t) \in [\tau_m, \tau_1]$ , 应用Jessen不等式得:

$$\begin{aligned} -\tau_m \int_{t-\tau_m}^t \dot{x}^T(s)R_1\dot{x}(s)ds \leq \\ \left[ \begin{array}{c} x(t) \\ x(t-\tau_m) \end{array} \right]^T \left[ \begin{array}{cc} -R_1 & R_1 \\ R_1 & -R_1 \end{array} \right] \left[ \begin{array}{c} x(t) \\ x(t-\tau_m) \end{array} \right], \quad (4) \end{aligned}$$

$$\begin{aligned} -\int_{t-\tau_2}^{t-\tau_1} \dot{x}^T(s)R_3\dot{x}(s)ds \leq \\ \frac{1}{\beta} \left[ \begin{array}{c} x(t-\tau_1) \\ x(t-\tau_2) \end{array} \right]^T \left[ \begin{array}{cc} -R_3 & R_3 \\ R_3 & -R_3 \end{array} \right] \left[ \begin{array}{c} x(t-\tau_1) \\ x(t-\tau_2) \end{array} \right], \quad (5) \end{aligned}$$

$$\begin{aligned} -\int_{t-\tau_m}^{t-\tau_2} \dot{x}^T(s)R_4\dot{x}(s)ds \leq \\ \frac{1}{\beta} \left[ \begin{array}{c} x(t-\tau_2) \\ x(t-\tau_m) \end{array} \right]^T \left[ \begin{array}{cc} -R_4 & R_4 \\ R_4 & -R_4 \end{array} \right] \left[ \begin{array}{c} x(t-\tau_2) \\ x(t-\tau_m) \end{array} \right]. \quad (6) \end{aligned}$$

引入如下自由权矩阵:

$$\begin{aligned} 2\xi^T(t)N_1[x(t-\tau_m) - x(t-\tau(t)) - \\ \int_{t-\tau(t)}^{t-\tau_m} \dot{x}^T(s)ds] = 0, \\ 2\xi^T(t)M_1[x(t-\tau(t)) - x(t-\tau_1) - \\ \int_{t-\tau_1}^{t-\tau(t)} \dot{x}^T(s)ds] = 0, \end{aligned}$$

且下列不等式成立:

$$\begin{aligned} -2\xi^T(t)N_1 \int_{t-\tau(t)}^{t-\tau_m} \dot{x}^T(s)ds \leq \\ (\tau(t) - \tau_m)\xi^T(t)N_1R_2^{-1}N_1^T\xi(t) + \end{aligned}$$

$$\begin{aligned} \int_{t-\tau(t)}^{t-\tau_m} \dot{x}^T(s)R_2\dot{x}(s)ds, \\ -2\xi^T(t)M_1 \int_{t-\tau(t)}^{t-\tau_m} \dot{x}^T(s)ds \leq \\ (\tau(t) - \tau_m)\xi^T(t)M_1R_2^{-1}M_1^T\xi(t) + \\ \int_{t-\tau(t)}^{t-\tau_m} \dot{x}^T(s)R_2\dot{x}(s)ds, \end{aligned}$$

则如下不等式成立:

$$\begin{aligned} \dot{V}(x_t) \leq & \xi^T(t)(\Phi_1 + \Xi_1^i + \Xi_1^{iT})\xi(t) + \\ & 2\xi^T(t)SB\mu_2\delta + \\ & (\tau(t) - \tau_m)\xi^T(t)NR_2^{-1}N^T\xi(t) + \\ & (\tau_1 - \tau(t))\xi^T(t)MR_2^{-1}M^T\xi(t). \quad (7) \end{aligned}$$

由引理1以及Schur补得如下两个不等式:

$$\begin{aligned} \dot{V}(x_t) \leq & \xi^T(t) \begin{bmatrix} H_1 & \beta M_1 \\ \beta M_1^T & -\beta R_2 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta, \\ \dot{V}(x_t) \leq & \xi^T(t) \begin{bmatrix} H_1 & \beta N_1 \\ \beta N_1^T & -\beta R_2 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta. \end{aligned}$$

由定理1得

$$\begin{aligned} \dot{V}(x_t) \leq & -\frac{\|\xi(t)\|^2}{\|T^{-1}\|} + 2\xi^T(t)SB\mu_2\delta = \\ & -\frac{\|\xi(t)\|}{\|T^{-1}\|}(\|\xi(t)\| - 2\mu_2\delta\|SB\|\|T^{-1}\|). \end{aligned}$$

由 $\delta$ 的定义, 可将 $\delta$ 表示成

$$\begin{aligned} \delta = & \mu_2^{-1}\mu_1K[\mu_1^{-1}x(t-\tau(t)) - q_1(\mu_1^{-1}x(t-\tau(t)))] + \\ & [\mu_2^{-1}K\mu_1q_1(\mu_1^{-1}x(t-\tau(t))) - \\ & q_2(\mu_2^{-1}K\mu_1q_1(\mu_1^{-1}x(t-\tau(t))))] \leqslant \\ & \|K\|\Delta_1 + \Delta_2 = \Delta. \end{aligned}$$

由量化器性质及定理1得

$$\begin{aligned} 2\Delta\|SB\|\|T^{-1}\| \leq & \mu_1^{-1}\|x(t)\| \leq F_1, \\ \|\mu_2^{-1}K\mu_1q_1(\mu_1^{-1}x(t))\| \leq & \|K\|(\Delta_1 + M_1) \leq F_2, \end{aligned}$$

则 $2\mu_2\delta\|SB\|\|T^{-1}\| \leq \xi(t)$ 成立.

因此 $\dot{V}(x_t) \leq 0$ , 定理1得证.

**情形2**  $\tau(t) \in [\tau_1, \tau_2]$ , 应用式(6)和如下Jessen不等式:

$$\begin{aligned} -\int_{t-\tau_1}^{t-\tau_m} \dot{x}^T(s)R_2\dot{x}(s)ds \leq \\ \frac{1}{\beta} \left[ \begin{array}{c} x(t-\tau_m) \\ x(t-\tau_1) \end{array} \right]^T \left[ \begin{array}{cc} -R_2 & R_2 \\ R_2 & -R_2 \end{array} \right] \left[ \begin{array}{c} x(t-\tau_m) \\ x(t-\tau_1) \end{array} \right]. \quad (8) \end{aligned}$$

引入如下自由权矩阵:

$$\begin{aligned} 2\xi^T(t)N_2[x(t-\tau_1) - \\ x(t-\tau(t)) - \int_{t-\tau(t)}^{t-\tau_1} \dot{x}^T(s)ds] = 0, \\ 2\xi^T(t)M_2[x(t-\tau(t))] - \end{aligned}$$

$$x(t - \tau_2) - \int_{t-\tau_2}^{t-\tau(t)} \dot{x}^T(s) ds = 0,$$

且下列不等式成立:

$$\begin{aligned} & -2\xi^T(t)N_2 \int_{t-\tau(t)}^{t-\tau_1} \dot{x}^T(s) ds \leq \\ & (\tau(t) - \tau_1)\xi^T(t)N_2R_3^{-1}N_2^T\xi(t) + \\ & \int_{t-\tau(t)}^{t-\tau_1} \dot{x}^T(s)R_3\dot{x}(s) ds, \\ & -2\xi^T(t)M_2 \int_{t-\tau_2}^{t-\tau(t)} \dot{x}^T(s) ds \leq \\ & (\tau_2 - \tau(t))\xi^T(t)M_2R_3^{-1}M_2^T\xi(t) + \\ & \int_{t-\tau_2}^{t-\tau(t)} \dot{x}^T(s)R_3\dot{x}(s) ds, \end{aligned}$$

则如下不等式成立:

$$\begin{aligned} \dot{V}(x_t) \leq & \xi^T(t)(\Phi_2 + \Xi_2 + \Xi_2^T)\xi(t) + 2\xi^T(t)SB\mu_2\delta + \\ & (\tau(t) - \tau_1)\xi^T(t)TR_3^{-1}T^T\xi(t) + \\ & (\tau_2 - \tau(t))\xi^T(t)VR_3^{-1}V^T\xi(t). \end{aligned}$$

由Schur补得等价于如下两个不等式:

$$\begin{aligned} \dot{V}(x_t) \leq & \xi^T(t) \begin{bmatrix} \Pi_2 & \beta M_2 \\ \beta M_2^T & -\beta R_3 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta, \\ \dot{V}(x_t) \leq & \xi^T(t) \begin{bmatrix} \Pi_2 & \beta N_2 \\ \beta N_2^T & -\beta R_3 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta. \end{aligned}$$

由量化器性质及定理1得 $\dot{V}(x_t) \leq 0$ , 定理1得证.

**情形3**  $\tau(t) \in [\tau_2, \tau_M]$ , 利用式(5)和(8)并引入自由权:

$$\begin{aligned} & 2\xi^T(t)N_3[x(t - \tau_2) - \\ & x(t - \tau(t)) - \int_{t-\tau(t)}^{t-\tau_2} \dot{x}^T(s) ds] = 0, \\ & 2\xi^T(t)M_3[x(t - \tau(t)) - \\ & x(t - \tau_M) - \int_{t-\tau_M}^{t-\tau(t)} \dot{x}^T(s) ds] = 0, \end{aligned}$$

且下列不等式成立:

$$\begin{aligned} & -2\xi^T(t)N_3 \int_{t-\tau(t)}^{t-\tau_2} \dot{x}^T(s) ds \leq \\ & (\tau(t) - \tau_2)\xi^T(t)N_3R_4^{-1}N_3^T\xi(t) + \\ & \int_{t-\tau(t)}^{t-\tau_2} \dot{x}^T(s)R_4\dot{x}(s) ds, \\ & -2\xi^T(t)M_3 \int_{t-\tau_M}^{t-\tau(t)} \dot{x}^T(s) ds \leq \\ & (\tau_M - \tau(t))\xi^T(t)M_3R_4^{-1}M_3^T\xi(t) + \\ & \int_{t-\tau_M}^{t-\tau(t)} \dot{x}^T(s)R_4\dot{x}(s) ds, \end{aligned}$$

则如下不等式成立:

$$\begin{aligned} \dot{V}(x_t) \leq & \xi^T(t)(\Phi_3 + \Xi_3 + \Xi_3^T)\xi(t) + 2\xi^T(t)SB\mu_2\delta + \\ & (\tau(t) - \tau_2)\xi^T(t)WR_4^{-1}T^T\xi(t) + \\ & (\tau_M - \tau(t))\xi^T(t)ZR_4^{-1}Z^T\xi(t). \end{aligned}$$

由Schur补得等价于如下两个不等式:

$$\dot{V}(x_t) \leq \xi^T(t) \begin{bmatrix} \Pi_3 & \beta M_3 \\ \beta M_3^T & -\beta R_4 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta,$$

$$\dot{V}(x_t) \leq \xi^T(t) \begin{bmatrix} \Pi_3 & \beta N_3 \\ \beta N_3^T & -\beta R_4 \end{bmatrix} \xi(t) + 2\xi^T(t)SB\mu_2\delta.$$

由量化器性质及定理1得 $\dot{V}(x_t) \leq 0$ . 证毕.

**注1** 在情形1, 情形2和情形3这3种不同情况下, 采用了不同的自由权矩阵和Jessen不等式进行分析, 并且区别利用了矩阵函数的凸性, 采用更多的时滞信息, 从而减小了分析的保守性.

#### 4 状态反馈控制器设计(State feedback controller design)

**定理2** 若存在矩阵 $\tilde{P} > 0$ ,  $T > 0$ ,  $\tilde{Q}_i > 0$ ,  $R_i(i = 1, \dots, 4) > 0$ ,  $\lambda_i(i = 2, \dots, 7)$ , 非奇异矩阵 $X$ , 以及适当维数的矩阵 $\tilde{M}_i$ ,  $\tilde{N}_i(i = 1, 2, 3)$ ,  $Y$ 使得下列线性矩阵不等式成立:

$$\begin{bmatrix} \tilde{\Pi}_k & * & * \\ \beta \tilde{M}_k^T & -\beta \tilde{R}_{k+1} & * \\ W_3^T & 0 & -T^{-1} \end{bmatrix} < 0, \quad (9)$$

$$\begin{bmatrix} \tilde{\Pi}_k & * & * \\ \beta \tilde{N}_k^T & -\beta \tilde{R}_{k+1} & * \\ W_3^T & 0 & -T^{-1} \end{bmatrix} < 0, \quad (10)$$

其中:  $k = 1, 2, 3$ ,

$$\tilde{\Pi}_k = \tilde{\Phi}_k + \tilde{\Xi}_1^k + \tilde{\Xi}_1^{kT},$$

$$W_1 = \tilde{Q}_1 + \tilde{Q}_2 + \tilde{Q}_3 + \tilde{Q}_4 - \tilde{R}_1 - AX^T - XA^T,$$

$$W_2 = \tau_m^2 \tilde{R}_1 + \beta \tilde{R}_2 + \beta \tilde{R}_3 + \beta \tilde{R}_4 + \lambda_7 X + \lambda_7 X^T,$$

$$W_3^T = \text{diag}\{\underbrace{X^T, \dots, X^T}_8\},$$

$$\tilde{\Xi}_1^1 = [0 \ \tilde{N}_1 \ -\tilde{N}_1 + \tilde{M}_1 \ \tilde{M}_1 \ 0 \ 0 \ 0],$$

$$\tilde{\Xi}_1^2 = [0 \ 0 \ \tilde{N}_2 - \tilde{M}_2 \ \tilde{M}_2 \ -\tilde{N}_2 \ 0 \ 0],$$

$$\tilde{\Xi}_1^3 = [0 \ 0 \ \tilde{N}_3 - \tilde{M}_3 \ 0 \ \tilde{M}_3 \ -\tilde{N}_3 \ 0],$$

$$\tilde{\Phi}_1 = \begin{bmatrix} \tilde{W}_1 & * & * & * & * & * & * & * \\ \tilde{L}_1 & \tilde{L}_7 & * & * & * & * & * & * \\ \tilde{L}_2 & \tilde{L}_8 & \tilde{L}_9 & * & * & * & * & * \\ \tilde{L}_3 & 0 & -\lambda_4 BY & \tilde{L}_B & * & * & * & * \\ \tilde{L}_4 & 0 & -\lambda_5 BY & \frac{\tilde{R}_3}{\beta} & \tilde{L}_C & * & * & * \\ \tilde{L}_5 & 0 & -\lambda_6 BY & 0 & \frac{\tilde{R}_4}{\beta} & \tilde{L}_D & * & * \\ \tilde{L}_6 & \lambda_2 X & \tilde{L}_A & \lambda_4 X & \lambda_5 X & \lambda_6 X & \tilde{W}_2 & * \\ W_3^T & 0 & 0 & 0 & 0 & 0 & 0 & -T^{-1} \end{bmatrix},$$

$$\tilde{\Phi}_2 = \begin{bmatrix} \tilde{W}_1 & * & * & * & * & * & * & * \\ \tilde{L}_1 & \hat{L}_7 & * & * & * & * & * & * \\ \tilde{L}_2 & \tilde{L}_8 & \tilde{L}_9 & * & * & * & * & * \\ \tilde{L}_3 & \frac{\tilde{R}_2}{\beta} - \lambda_4 BY & \hat{L}_B & * & * & * & * & * \\ \tilde{L}_4 & 0 & -\lambda_5 BY & 0 & \hat{L}_C & * & * & * \\ \tilde{L}_5 & 0 & -\lambda_6 BY & 0 & 0 & \tilde{L}_D & * & * \\ \tilde{L}_6 & \lambda_2 X & \tilde{L}_A & \lambda_4 X & \lambda_5 X & \lambda_6 X & \tilde{W}_2 & * \\ W_3^T & 0 & 0 & 0 & 0 & 0 & 0 & -T^{-1} \end{bmatrix},$$
  

$$\tilde{\Phi}_3 = \begin{bmatrix} \tilde{W}_1 & * & * & * & * & * & * & * \\ \tilde{L}_1 & \hat{L}_7 & * & * & * & * & * & * \\ \tilde{L}_2 & \tilde{L}_8 & \tilde{L}_9 & * & * & * & * & * \\ \tilde{L}_3 & \frac{\tilde{R}_2}{\beta} - \lambda_4 BY & \tilde{L}_B & * & * & * & * & * \\ \tilde{L}_4 & 0 & -\lambda_5 BY & \frac{\tilde{R}_3}{\beta} & \tilde{L}_C & * & * & * \\ \tilde{L}_5 & 0 & -\lambda_6 BY & 0 & 0 & \tilde{L}_D & * & * \\ \tilde{L}_6 & \lambda_2 X & \tilde{L}_A & \lambda_4 X & \lambda_5 X & \lambda_6 X & \tilde{W}_2 & * \\ W_3^T & 0 & 0 & 0 & 0 & 0 & 0 & -T^{-1} \end{bmatrix},$$
  

$$\tilde{L}_1 = \tilde{R}_1 - \lambda_2 X^T, \quad \tilde{L}_2 = -\lambda_3 A X^T - Y^T B^T,$$

$$\tilde{L}_3 = -\lambda_4 A X^T, \quad \tilde{L}_4 = -\lambda_5 A X^T, \quad \tilde{L}_5 = -\lambda_6 A X^T,$$

$$\tilde{L}_6 = -\lambda_7 A X^T + X + \tilde{P}, \quad \tilde{L}_7 = -\tilde{Q}_1 - \tilde{R}_1,$$

$$\tilde{L}_8 = -\lambda_2 Y^T B^T, \quad \tilde{L}_9 = -\lambda_3 Y^T B^T - \lambda_3 B Y,$$

$$\tilde{L}_A = -\lambda_7 B Y + \lambda_3 X, \quad \tilde{L}_B = -\tilde{Q}_2 - \frac{\tilde{R}_3}{\beta},$$

$$\tilde{L}_C = -\tilde{Q}_3 - \frac{\tilde{R}_3}{\beta} - \frac{\tilde{R}_4}{\beta}, \quad \tilde{L}_D = -\tilde{Q}_4 - \frac{\tilde{R}_4}{\beta},$$

$$\hat{L}_B = -\tilde{Q}_2 - \frac{\tilde{R}_2}{\beta}, \quad \hat{L}_C = -\tilde{Q}_3 - \frac{\tilde{R}_4}{\beta},$$

$$\check{L}_B = -\tilde{Q}_2 - \frac{\tilde{R}_2}{\beta} - \frac{\tilde{R}_3}{\beta}, \quad \check{L}_C = -\tilde{Q}_3 - \frac{\tilde{R}_3}{\beta},$$

且量化器满足如下两个条件:

$$2\Delta \| [X^{-T} \lambda_2 X^{-T} \lambda_3 X^{-T} \lambda_4 X^{-T} \lambda_5 X^{-T} \lambda_6 X^{-T} \lambda_7 X^{-T}]^T B \| \| T^{-1} \| \leq \frac{\| x(t) \|}{\mu_2} \leq F_1;$$

$$F_2 \geq \| Y X^{-T} \| (\Delta_1 + F_1),$$

则系统(1)渐近稳定, 且控制器为  $K = Y X^{-T}$ .

证 令  $S^T = [S_1^T \ S_2^T \ S_3^T \ S_4^T \ S_5^T \ S_6^T \ S_7^T]$ , 将不等式(2)和(3)展开, 并令  $S_1 = X^{-1}$ ,  $S_j = \lambda_j X^{-1}$  ( $j = 2, \dots, 7$ ), 对式(2)和(3)两边分别左乘和右乘  $\text{diag}\{\underbrace{X, \dots, X}_{8}, I\}$  和其转置, 令

$$X P X^T = \tilde{P}, \quad X Q X^T = \tilde{Q},$$

$$X Q_i X = \tilde{Q}_i, \quad X R_i X = \tilde{R}_i, \quad i = 1, \dots, 4,$$

并令  $Y = K X^T$ , 则定理2得证. 证毕.

## 5 数值例子(Numerical examples)

### 例1 系统

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 \\ 0 & -0.1 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 0.1 \end{bmatrix} u(t),$$

给定反馈增益矩阵  $K = [-3.75 \ -11.5]$ , 不考虑量化的影响, 即  $\delta = 0$ , 通过定理1, 利用LMI工具箱, 可求得保证系统渐近稳定的时延上界. 从表1可以看出, 本文所述方法所带来的保守性远远小于文献[3]所述方法.

表1 不同时延下界情况下的最大时延上界

Table 1 Upper delay bound for different lower bound

$\tau_m$	0.0000	0.0100	0.0500	0.1000	0.2000
定理1	1.8090	1.8020	1.7740	1.7380	1.6640
文献[3]	0.9410	0.9421	0.9475	0.9520	0.9635

### 例2 系统

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 \\ -0.68 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} K x(t - \tau(t)),$$

考虑量化的影响, 通过定理2, 利用LMI工具箱, 选择  $\lambda_2 = 0.2, \lambda_3 = 2, \lambda_4 = 3, \lambda_5 = 4, \lambda_6 = 5, \lambda_7 = 10, T = I$ , 得  $\tau_M = 0.627, K = [0.0226 \ -1.18]$ ,

$$X = \begin{bmatrix} -1.5980 & 0.4960 \\ -0.4006 & -0.6226 \end{bmatrix},$$

则  $F_1 \geq 34.91\Delta, F_2 \geq 1.18(\Delta_1 + F_1)$ , 取  $\Delta_1 = \Delta_2 = 0.1$ , 则  $\frac{\| x(t) \|}{\mu_1} \geq 3.491, \delta = 0.22$ , 时变量化器变量  $\mu_1 = \mu_2$  随着  $x(t)$  的变化而变化, 假设  $x(0) = [0.3 \ 0]^T$ , 图2为有量化和无量化作用下的系统状态响应曲线和控制输入曲线图, 从图可以看出在状态量快速变化期间, 量化作用最大, 在状态量趋于稳定期间, 量化精度大.

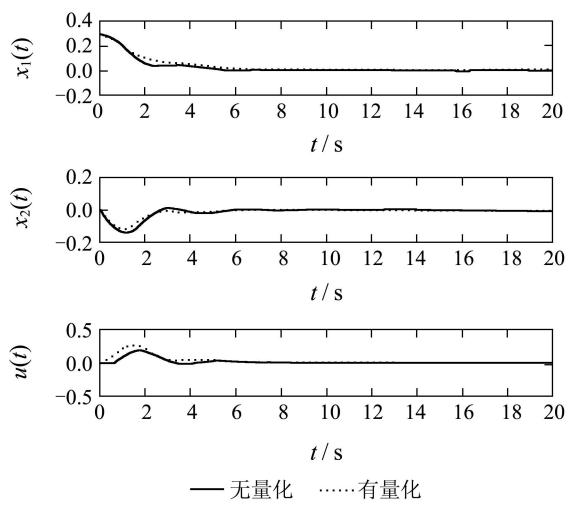


图2 系统状态响应和控制输入曲线图

Fig. 2 State response and control input of the system

## 6 结论(Conclusions)

本文采用分段时滞方法研究了时滞依赖的网络控制系统的量化控制。首先在系统中增加两个时变量化器,建立新的系统模型,其次通过将区间时变网络时滞分成3段,对每一段采用不同的分析方法,利用时滞的更多信息,从而得到了更好的结果。

## 参考文献(References):

- [1] ZHANG W, BRANICKY M S, PHILLIPS S M. Stability of networked control systems[J]. *IEEE Control System Magazine*, 2001, 21(11): 84–99.
- [2] YUE D, HAN Q L, PENG C. State feedback controller design of networked control systems[J]. *IEEE Transactions on Circuits and Systems*, 2004, 51(11): 640–644.
- [3] PENG C, TIAN Y C, TADE M O. State Feedback controller design of networked control systems with interval time-varying delay and non-linearity[J]. *International Journal of Robust and Nonlinear Control*, 2008, 18(12): 1285–1301.
- [4] YUE D, HAN Q L. Delayed feedback control of uncertain systems with time-varying input delay[J]. *Automatica*, 2005, 41(2): 233–240.
- [5] YUE D, HAN Q L, LAM J. Network-based robust control of systems with uncertainty[J]. *Automatica*, 2005, 41(6): 999–1007.
- [6] LIU J L, HU S L, TIAN E G. A novel method of  $H_\infty$  filter design for time-varying delay systems[J]. *ICIC Express Letters*, 2010, 4(3): 667–673.
- [7] YUE D, TIAN E G, ZHANG Y. A piecewise analysis method to stability analysis of linear continuous/discrete systems with time-varying delay[J]. *International Journal of Robust and Nonlinear Control*, 2009, 19(13): 1493–1518.
- [8] 谢林柏, 丁峰, 王艳. 基于辅助模型的量化控制系统辨识方法[J]. 控制理论与应用, 2009, 26(3): 277–282.  
(XIE Linbo, DING Feng, WANG Yan. Auxiliary model-based identification method for quantized control systems[J]. *Control Theory & Applications*, 2009, 26(3): 277–282.)
- [9] TIAN E G, YUE D, PENG C. Quantized output feedback control for networked control systems[J]. *Information Sciences*, 2008, 178(12): 2734–2749.
- [10] NIU Y, JIA T, WANG X, et al. Output-feedback control design for NCSs subject to quantization and dropout[J]. *Information Sciences*, 2009, 179(21): 3804–3813.
- [11] 褚红燕, 费树岷, 岳东. 基于T-S模型的非线性网络控制系统的量化保成本控制[J]. 控制与决策, 2010, 25(1): 31–36.  
(CHU Hongyan, FEI Shumin, YUE Dong. Quantized guaranteed cost control for T-S fuzzy nonlinear networked control systems[J]. *Control and Decision*, 2010, 25(1): 31–36.)

## 作者简介:

- 褚红燕** (1979—), 女, 博士研究生, 目前研究方向为网络控制系统, E-mail: njnuchuhongyan@163.com;
- 费树岷** (1961—), 男, 教授, 博士生导师, 目前研究方向为非线性系统, E-mail: smfei@seu.edu.cn;
- 刘金良** (1980—), 男, 博士研究生, 目前研究方向为时滞系统控制, E-mail: liujinliang@vip.163.com;
- 翟军勇** (1977—), 男, 博士, 副教授, 目前研究方向为时滞系统设计, E-mail: jyzhai@163.com.