网络化不确定系统集中式融合鲁棒稳态估值器

陶贵丽¹,李 爽²,刘文强^{2†}

(1. 浙江传媒学院 媒体工程学院, 浙江 杭州 310018;

2. 浙江工商大学 信息与电子工程学院(萨塞克斯人工智能学院), 浙江 杭州 310018)

摘要:对于一类在状态转移阵和系统观测阵中带相同的状态依赖乘性噪声、带噪声依赖乘性噪声、一步随机观 测滞后、丢包和不确定噪声方差的多传感器网络化系统,文章研究其鲁棒集中式融合稳态滤波问题.应用增广方法 将系统转换为带随机参数矩阵、相同过程和观测噪声的集中式融合系统.应用去随机化方法和虚拟噪声技术,系统 进一步转化为仅带不确定噪声方差的集中式融合系统.根据极大极小鲁棒估计原理,本文提出了鲁棒集中式融合稳 态Kalman估值器(预报器、滤波器和平滑器),证明了所提出的集中式融合估值器的鲁棒性,给出了鲁棒局部与集中 式融合估值器之间的精度关系.本文提出了应用于多传感器多通道滑动平均(MA)信号估计的一个实例,给出了相 应的鲁棒局部和集中式融合信号估值器.仿真实验验证了所提出方法的有效性和正确性.

关键词:集中式融合;鲁棒稳态估值器;一步随机滞后;丢包;不确定噪声方差;极大极小鲁棒估计原理

引用格式: 陶贵丽, 李爽, 刘文强. 网络化不确定系统集中式融合鲁棒稳态估值器. 控制理论与应用, 2023, 40(8): 1466 – 1478

DOI: 10.7641/CTA.2022.20093

Centralized fusion robust steady-state estimators for networked uncertain systems

TAO Gui-li¹, LI Shuang², LIU Wen-qiang^{2†}

 College of Media Engineering, Communication University of Zhejiang, Hangzhou Zhejiang 310018, China;
 School of Information and Electronic Engineering (Sussex Artificial Intelligence Institute), Zhejiang Gongshang University, Hangzhou Zhejiang 310018, China)

Abstract: The centralized fusion (CF) robust steady-state filtering problem is investigated for a class of multisensor networked systems with mixed uncertainties. The uncertainties include the same state-dependent multiplicative noises in state transition and system measurement matrices, noise-dependent multiplicative noises, one-step random delay, packet dropouts, and uncertain noise variances. By means of the augmentation approach, the system under study is converted into one with random parameter matrices and same process and measurement noises. Using the de-randomization approach and fictitious noise technique, the system is further converted into one with only uncertain noise variances. In the light of the minimax robust estimation principle, the robust CF steady-state Kalman estimators (predictor, filter, and smoother) are presented. The robustness of the proposed CF estimators is proved, the accuracy relations among the robust local and CF steady-state Kalman estimators are given. An example with application to multisensor multichannel moving average (MA) signal estimate is proposed, and the corresponding robust local and CF signal estimators are given. Simulation example verifies the effectiveness and correctness of the proposed method.

Key words: centralized fusion; robust steady-state estimators; one-step random delay; packet dropouts; uncertain noise variances; minimax robust estimation principle

Citation: TAO Guili, LI Shuang, LIU Wenqiang. Centralized fusion robust steady-state estimators for networked uncertain systems. *Control Theory & Applications*, 2023, 40(8): 1466 – 1478

收稿日期: 2022-02-02; 录用日期: 2022-08-02.

[†]通信作者. E-mail: lwq@zjgsu.edu.cn; Tel.: +86 17367114907.

本文责任编委: 周杰.

黑龙江省自然科学基金项目(LH2019F035),国家自然科学基金项目(61803148),浙江省教育厅科研项目(Y202147323),浙江传媒学院人才引进科研与创作项目(Z301B19539)资助.

Supported by the Natural Science Foundation of Heilongjiang Province (LH2019F035), the National Natural Science Foundation of China (618031 48), the Scientific Research Project of Zhejiang Provincial Education Department (Y202147323) and the Scientific Research and Creative Project of Communication University of Zhejiang (Z301B19539).

1 引言

多传感器信息融合技术可以利用所有传感器的信息,克服了单传感器受时间和空间限制的缺陷,现已 被广泛应用于目标跟踪、导航制导、信号处理等热门领域^[1].

近年来, 网络化系统的滤波问题受到广泛关注^[2-4]. 众所周知, 经典Kalman滤波方法要求系统的 模型参数和噪声方差是精确己知的^[5], 但在实际应用 中, 由于建模误差或未建模动态以及随机扰动等原因, 导致系统模型是不确定的^[6-17]. 当系统模型中存在不 确定性时, Kalman滤波器的性能会严重变坏, 甚至导 致滤波发散. 解决这一问题的方法之一是设计鲁 棒Kalman滤波器, 即针对由不确定性所描述的一族系 统模型来设计一个滤波器, 使得对所有容许的不确定 性, 滤波器的实际滤波误差方差确保有一个最小上 界^[17].

在网络化系统中,信道中会不可避免地存在不确 定性,例如随机观测滞后与丢包,估值器的性能会受 其影响^[18]. 这类不确定性的存在会导致估值器接收到 的数据出现偏差. 伯努利随机变量序列是描述这类不 确定性的常用工具^[19-21].

随机参数不确定性可以用乘性噪声来描述,对确 定性参数的随机扰动称为乘性噪声,包括状态依赖和 噪声依赖乘性噪声. 在系统状态和观测矩阵中的白噪 声称为状态依赖乘性噪声,在噪声转移矩阵中的白噪 声称为噪声依赖乘性噪声.噪声方差的不确定性可以 通过确定的不确定性来描述,即噪声方差是未知不确 定的,但有已知的保守上界[14-17].近年来,对于带乘 性噪声、不确定噪声方差、随机观测滞后和丢包的网 络化系统,鲁棒或最优状态估计问题已被广泛研 究[15-17,22-28]. 文献[22]中,针对系统状态和观测矩阵 中带乘性噪声并具有多步随机观测滞后和丢包的不 确定网络化系统,通过射影理论,提出了最小方差意 义下的最优线性估值器. 文献[23]中, 针对带乘性噪 声、一步随机观测滞后和丢包的网络化控制系统,其 中传感器到估值器和控制器到执行器的通道都受到 乘性噪声影响,利用射影理论推导出了最优估值器. 但文献[22-23]的结果都局限于单传感器系统.

对于在系统状态和观测矩阵中带乘性噪声,并具 有一步随机传输时滞和丢包的混合不确定多传感器 网络化系统,文献[24]基于矩阵加权融合算法提出了 一种分布式融合滤波器.对于一类在状态转移矩阵中 存在乘性噪声,并具有丢失观测、随机观测滞后和丢 包的不确定多传感器网络化系统,应用新息分析方法, 文献[25]提出了鲁棒集中式融合以及降维观测融合 Kalman滤波器,但文献[25]没有考虑系统观测矩阵中 的乘性噪声. 文献[26]中, 针对带随机参数矩阵、一步随机观测滞后和丢包的多传感器网络化系统, 提出了局部最小二乘线性估值器(滤波器和固定点平滑器), 并利用矩阵加权融合算法得到了分布式融合滤波器和平滑器. 然而, 文献[22-26]均没有考虑噪声依赖乘 性噪声, 且都假定系统噪声方差是精确已知的.

针对在系统状态和观测矩阵中带乘性噪声,并带 丢包和不确定噪声方差的多传感器网络化系统,文献 [27]提出了加权状态融合鲁棒Kalman估值器. 但文献 [27]中没有考虑随机观测滞后不确定性. 对系统状态 和观测矩阵中存在乘性噪声,并具有一步随机观测滞 后和不确定噪声方差的多传感器网络化系统, 文献 [28]提出了综合协方差交叉融合鲁棒Kalman估值器. 文献[15]针对在系统状态与观测矩阵中存在相同乘性 噪声,以及带一步随机观测滞后、丢失观测、以及不确 定噪声方差的多传感器网络化系统,利用极大极小鲁 棒估计准则,提出了鲁棒矩阵加权和集中式融合稳 态Kalman估值器. 文献[16]中,针对带乘性噪声、两 步随机观测滞后、丢失观测和不确定噪声方差的多传 感器网络化系统,提出了鲁棒集中式融合和加权观测 融合稳态Kalman估值器. 文献[15-16]提出的鲁棒融 合滤波方法可用于解决带有色观测噪声的多传感 器单通道自回归信号的鲁棒融合滤波问题.但文献 [15-16,27-28]中均没有考虑噪声依赖乘性噪声. 对于 系统状态和过程噪声转移矩阵中带乘性噪声,并具有 不确定噪声方差、一步随机观测滞后和丢失观测的多 传感器网络化系统, 文献[29]提出了鲁棒局部和5种融 合时变Kalman估值器(预报器、滤波器和平滑器). 但 文献 [29] 中没有考虑系统观测矩阵中的乘性噪声, 且文献[15-16,28-29]都没有考虑丢包. 此外, 与文献 [15-16]相比, 文献[28-29]中用到的增广方法会使系 统状态转移矩阵具有较大维数. 对一类系统所有参数 矩阵中带相同乘性噪声,并带一步随机观测滞后和不 连续丢包的多传感器网络化系统,根据极大极小鲁棒 估计原理,文献[17]提出了鲁棒矩阵加权融合稳 态Kalman估值器. 但文献[17]中没有考虑丢包补偿机 制以及集中式融合滤波问题,基于上述分析,对于在 系统状态和观测矩阵中带相同状态依赖乘性噪声,并 带噪声依赖乘性噪声、不确定噪声方差、一步随机观 测滞后和丢包的多传感器网络化系统,其鲁棒集中式 融合稳态滤波问题尚未见报道.因此,本文对此进行 研究.

本文的主要创新点如下:1) 对于所研究的系统模型,给出了其集中式融合鲁棒稳态估值器存在的充分 条件,并基于极大极小鲁棒估计原理提出了集中式融 合鲁棒稳态Kalman估值器(预报器、滤波器和平滑 器);2) 应用增广方法、非负定矩阵分解方法和李雅普 诺夫方程方法,证明了所提出的集中式融合估值器的 鲁棒性;3)给出了一个应用于多传感器多通道滑动平 均(moving average, MA)信号估计的例子,解决了带 随机参数矩阵的多通道MA信号的集中式融合估计问 题,得到了相应的鲁棒局部和集中式融合稳态信号估 值器.

2 问题描述

考虑如下线性离散不确定多传感器网络化系统:

$$x(t+1) = (\Phi + \sum_{k=1}^{n_{\alpha}} \alpha_k(t)\Phi_k)x(t) + (\Gamma + \sum_{k=1}^{n_{\beta}} \beta_k(t)\Gamma_k)w(t),$$
(1)

$$z_i(t) = (H_i + \sum_{k=1}^{n_{\alpha}} \alpha_k(t) H_{ik}) x(t) + v_i(t), \qquad (2)$$

$$v_i(t) = D_i w(t) + \eta_i(t), \qquad (3)$$

$$y_{i}(t) = \xi_{i}(t)z_{i}(t) + (1 - \xi_{i}(t))\zeta_{i}(t)z_{i}(t - 1) + (1 - \xi_{i}(t))(1 - \zeta_{i}(t))y_{i}(t - 1),$$

$$i = 1, \cdots, L,$$
(4)

其中: t是离散时间; $x(t) \in \mathbb{R}^n$ 是被估状态; $z_i(t) \in \mathbb{R}^{m_i}$ 是传感器接收到的观测; $y_i(t) \in \mathbb{R}^{m_i}$ 是估值器接收到 的观测; $w(t) \in \mathbb{R}^r$ 是过程噪声; $v_i(t) \in \mathbb{R}^{m_i}$ 是观测噪 声且线性相关于w(t); $\alpha_k(t) \in \mathbb{R}^1$, $k = 1, \cdots, n_\alpha$ 是 状态依赖乘性噪声; $\beta_k(t) \in \mathbb{R}^1$, $k = 1, \cdots, n_\beta$ 是噪声 依赖乘性噪声; $\Phi \in \mathbb{R}^{n \times n}$, $\Phi_k \in \mathbb{R}^{n \times n}$, $\Gamma \in \mathbb{R}^{n \times r}$, $\Gamma_k \in \mathbb{R}^{n \times r}$, $H_i \in \mathbb{R}^{m_i \times n}$, $H_{ik} \in \mathbb{R}^{m_i \times n}$ 和 $D_i \in \mathbb{R}^{m_i \times r}$ 是具有 适当维数的已知常矩阵; Φ_k , Γ_k 和 H_{ik} 是扰动方位矩 阵; n_α , n_β 是相应乘性噪声的数目; L是传感器的数 目.

 $\xi_i(t) \in \mathbb{R}^1 \pi \zeta_i(t) \in \mathbb{R}^1, i = 1, \dots, L$ 是 取 值 为0 或1的各自不相关伯努利白噪声,具有已知概率 $\operatorname{Prob}(\xi_i(t) = 1) = \pi_i, \operatorname{Prob}(\xi_i(t) = 0) = 1 - \pi_i,$ $\operatorname{Prob}(\zeta_i(t) = 1) = \varsigma_i, \operatorname{Prob}(\zeta_i(t) = 0) = 1 - \varsigma_i, 其$ $+\pi_i \pi_{\varsigma_i}$ 是已知的, $\pm 0 \leq \pi_i \leq 1, 0 \leq \varsigma_i \leq 1. \xi_i(t)$ 和 $\zeta_i(t)$ 也不相关于其他随机信号. 容易得到以下结论:

$$E[\xi_{i}(t)] = \pi_{i}, E[\xi_{i}^{2}(t)] = \pi_{i},$$

$$E[(\xi_{i}(t) - \pi_{i})^{2}] = \pi_{i}(1 - \pi_{i}),$$

$$E[(\xi_{i}(t) - \pi_{i})(\xi_{j}(t) - \pi_{j})] = 0, i \neq j,$$

$$E[\zeta_{i}(t)] = \varsigma_{i}, E[\zeta_{i}^{2}(t)] = \varsigma_{i},$$

$$E[(\zeta_{i}(t) - \varsigma_{i})^{2}] = \varsigma_{i}(1 - \varsigma_{i}),$$

$$E[(\zeta_{i}(t) - \varsigma_{i})(\zeta_{j}(t) - \varsigma_{j})] = 0, i \neq j.$$
(5)

假设1 $w(t), \eta_i(t), \alpha_k(t)$ 和 $\beta_k(t)$ 是具有零 均值的互不相关白噪声,它们的协方差为

$$\begin{split} \mathbf{E}[w(t)w^{\mathrm{T}}(u)] &= \bar{Q}\delta_{tu}, \\ \mathbf{E}[\eta_i(t)\eta_j^{\mathrm{T}}(u)] &= \bar{R}_{\eta_i}\delta_{ij}\delta_{tu} \end{split}$$

$$\begin{split} \mathbf{E}[\alpha_k(t)\alpha_h^{\mathrm{T}}(u)] &= \bar{\sigma}_{\alpha_k}^2 \delta_{kh} \delta_{tu}, \\ \mathbf{E}[\beta_k(t)\beta_h^{\mathrm{T}}(u)] &= \bar{\sigma}_{\beta_k}^2 \delta_{kh} \delta_{tu}, \end{split}$$

其中: \bar{Q} , \bar{R}_{η_i} , $\bar{\sigma}^2_{\alpha_k}$ 和 $\bar{\sigma}^2_{\beta_k}$ 分别是白噪声w(t), $\eta_i(t)$, $\alpha_k(t)$ 和 $\beta_k(t)$ 的未知不确定实际(真实)方差, δ_{kj} 表示 Kronecker 函数, $\delta_{kk} = 1$, $\delta_{kj} = 0(k \neq j)$.

假设2 初始状态 x(0) 不相关于 w(t), $\eta_i(t)$, $\alpha_k(t)$, $\beta_k(t)$, $\xi_i(t)$ 和 $\zeta_i(t)$, 且E[x(0)] = μ_0 , 其中: μ_0 是 x(0)的均值, E[$(x(0) - \mu_0)(x(0) - \mu_0)^{\mathrm{T}}$] = \bar{P}_0 , \bar{P}_0 是 x(0)的未知不确定实际方差.

假设3 $Q, R_{\eta_i}, \sigma^2_{\alpha_k}, \sigma^2_{\beta_k}$ 和 P_0 分别是 $\bar{Q}, \bar{R}_{\eta_i}, \bar{\sigma}^2_{\alpha_k}, \bar{\sigma}^2_{\beta_k}$ 和 \bar{P}_0 的已知保守上界,即满足

$$\bar{Q} \leqslant Q, \ \bar{R}_{\eta_i} \leqslant R_{\eta_i}, \ \bar{\sigma}_{\alpha_k}^2 \leqslant \sigma_{\alpha_k}^2, \ \bar{\sigma}_{\beta_k}^2 \leqslant \sigma_{\beta_k}^2, \ \bar{P}_0 \leqslant P_0.$$
(6)

注 1 带未知不确定实际方差 \bar{Q} , \bar{R}_{η_i} , $\bar{\sigma}^2_{\alpha_k}$, $\bar{\sigma}^2_{\beta_k}$ 和 \bar{P}_0 的系统(1)-(4)称为实际系统,带已知保守上界Q, R_{η_i} , $\sigma^2_{\alpha_k}$, $\sigma^2_{\beta_k}$ 和 P_0 的系统(1)-(4)称为最坏情形保守系统."最坏情形"系统是指带最大噪声和初始状态方差的系统.针对"最坏情形"系统的"最小"方差估值器称为极大极小鲁棒估值器,这就是极大极小鲁棒估计原理.

问题是对不确定多传感器网络化系统(1)–(4)中的状态x(t),设计鲁棒集中式融合稳态 Kalman 估值器 $\hat{x}_c(t|t+N)$,使得对于所有容许的不确定性,它们的实际稳态估计误差方差 $\bar{P}_c(N)$ 有相应的最小上界 $P_c(N)$,即 $\bar{P}_c(N) \leqslant P_c(N)$,下角标"c"表示集中式融合,N = -1, N = 0和N > 0分别表示一步预报器,滤波器和平滑器.

注 2 在式(4)中, 白噪声 $\xi_i(t)$ 和 $\zeta_i(t)$ 被用来描述一步随机观测滞后和丢包. 如果 $\xi_i(t) = 1$, 则 $y_i(t) = z_i(t)$ (没有观测滞后和丢包); 如果 $\xi_i(t) = 0$ 且 $\zeta_i(t) = 1$, 则 $y_i(t) = z_i(t-1)$ (一步随机观测滞后); 如果 $\xi_i(t) = 0$ 且 $\zeta_i(t) = 0$, 则 $y_i(t) = y_i(t-1)$ (丢包), 即观测 $z_i(t)$ 丢失, 但估值器在t - 1时刻接收到的观测 $y_i(t-1)$ 被用来作为t时刻的补偿, 这称为保持输入补偿机制. 这不同于文献[17]中的零输入补偿机制, 即如果当前时刻传感器观测丢失, 则估值器的观测将被置为0.

3 模型转换

3.1 增广集中式融合系统

合并式(2)给出的所有传感器输出向量,得到如下 增广观测输出方程:

 $\begin{array}{c} \prod_{k=1}^{n} \prod_{k=1}^{n$

将式(2)代入式(4)中,然后合并所有由式(4)给出

的估值器收到的观测向量可得

$$y^{(c)}(t) = \xi(t)(H^{(c)} + \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t)H^{(c)}_{k})x(t) + \xi(t) \times v^{(c)}(t) + (I_{m} - \xi(t))\zeta(t)z^{(c)}(t-1) + (I_{m} - \xi(t))(I_{m} - \zeta(t))y^{(c)}(t-1), \quad (8)$$

其中: $y^{(c)}(t) = [y_1^{\mathrm{T}}(t) \cdots y_L^{\mathrm{T}}(t)]^{\mathrm{T}}, m = \sum_{i=1}^{L} m_i, \xi(t) =$ diag{ $\xi_1(t)I_{m_1}, \cdots, \xi_L(t)I_{m_L}$ }, $\zeta(t) =$ diag{ $\zeta_1(t)I_{m_1}, \cdots, \zeta_L(t)I_{m_L}$ }, $I_m =$ diag{ I_{m_1}, \cdots, I_{m_L} }.

应用式(1)(7)-(8)可得如下增广集中式融合系统:

$$x_a(t+1) = \Phi_a(t)x_a(t) + \Gamma_a(t)w_a(t),$$
 (9)

$$y^{(c)}(t) = H_a(t)x_a(t) + G_a(t)w_a(t),$$
 (10)

其中:

$$\begin{cases} x_{a}(t) = \begin{bmatrix} x(t) \\ z^{(c)}(t-1) \\ y^{(c)}(t-1) \end{bmatrix}, w_{a}(t) = \begin{bmatrix} w(t) \\ v^{(c)}(t) \end{bmatrix}, \\ \Phi_{a}(t) = \begin{bmatrix} \Phi + \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) \Phi_{k} \\ H^{(c)} + \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) H^{(c)}_{k} \\ \xi(t)(H^{(c)} + \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) H^{(c)}_{k}) \\ (0)_{n \times m} \qquad (0)_{n \times m} \\ (0)_{m \times m} \qquad (0)_{m \times m} \\ (0)_{m \times m} \qquad (0)_{m \times m} \\ (I_{m} - \xi(t))\zeta(t) \qquad (I_{m} - \xi(t))(I_{m} - \zeta(t)) \end{bmatrix}, \\ \Gamma_{a}(t) = \begin{bmatrix} \Gamma + \sum_{k=1}^{n_{\beta}} \beta_{k}(t)\Gamma_{k} \qquad (0)_{n \times m} \\ (0)_{m \times r} \qquad I_{m} \\ (0)_{m \times r} \qquad \xi(t) \end{bmatrix}, \\ H_{a}(t) = [\xi(t)(H^{(c)} + \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t)H^{(c)}_{k}) \\ (I_{m} - \xi(t))\zeta(t) \qquad (I_{m} - \xi(t))(I_{m} - \zeta(t))], \\ G_{a}(t) = [(0)_{m \times r} \qquad \xi(t)]. \end{cases}$$
(11)

增广集中式融合系统(9)-(10)可进一步被转化为带常 参数矩阵和乘性噪声的系统形式,即

$$x_{a}(t+1) = (\Phi_{a}^{m} + \sum_{k=1}^{n_{a}} \alpha_{k}(t) \Phi_{a}^{\alpha k} + \sum_{i=1}^{L} \xi_{iz}(t) \times \Phi_{a}^{\xi i} + \sum_{i=1}^{L} \zeta_{iz}(t) \Phi_{a}^{\zeta i} + \sum_{i=1}^{L} \gamma_{iz}(t) \Phi_{a}^{\gamma i} + \sum_{i=1}^{L} \xi_{iz}(t) \sum_{k=1}^{n_{a}} \alpha_{k}(t) \Phi_{a}^{ki} x_{a}(t) + (\Gamma_{a}^{m} + \sum_{k=1}^{n_{\beta}} \beta_{k}(t) \Gamma_{a}^{\beta k} + \sum_{i=1}^{L} \xi_{iz}(t) \Gamma_{a}^{\xi i} w_{a}(t),$$
(12)

$$y^{(c)}(t) = (H_a^m + \sum_{k=1}^{n_\alpha} \alpha_k(t) H_a^{\alpha k} + \sum_{i=1}^{L} \xi_{iz}(t) H_a^{\xi i} + \sum_{i=1}^{L} \zeta_{iz}(t) H_a^{\zeta i} + \sum_{i=1}^{L} \gamma_{iz}(t) H_a^{\gamma i} + \sum_{i=1}^{L} \xi_{iz}(t) \times \sum_{k=1}^{n_\alpha} \alpha_k(t) H_a^{ki} x_a(t) + (G_a^m + \sum_{i=1}^{L} \xi_{iz}(t) G_a^{\xi i}) w_a(t),$$
(13)

其中:

$$\begin{split} &\Pi = \mathrm{E}\left[\xi(t)\right] = \mathrm{diag}\left\{\pi_{1}I_{m_{1}}, \cdots, \pi_{L}I_{m_{L}}\right\}, \\ &\Xi = \mathrm{E}[\zeta(t)] = \mathrm{diag}\left\{\varsigma_{1}I_{m_{1}}, \cdots, \varsigma_{L}I_{m_{L}}\right\}, \\ &\Phi_{a}^{m} = \begin{bmatrix} \Phi & (0)_{n \times m} & (0)_{n \times m} \\ H^{(c)} & (0)_{m \times m} & (0)_{m \times m} \\ \Pi H^{(c)} & (I_{m} - \Pi)\Xi & (I_{m} - \Pi)(I_{m} - \Xi) \end{bmatrix} \right] \\ &\Gamma_{a}^{m} = \begin{bmatrix} \Pi H^{(c)} & (I_{m} - \Pi)\Xi & (I_{m} - \Pi)(I_{m} - \Xi) \end{bmatrix}, \\ &H_{a}^{m} = [\Pi H^{(c)} & (I_{m} - \Pi)\Xi & (I_{m} - \Pi)(I_{m} - \Xi)], \\ &G_{a}^{m} = [(0)_{m \times r} & \Pi], \\ &N_{i} = & \mathrm{diag}\left\{(0)_{m_{1} \times m_{1}}, \cdots, (0)_{m_{i-1} \times m_{i-1}}, I_{m_{i}}, \\ & (0)_{m_{i+1} \times m_{i+1}}, & \cdots, (0)_{m_{L} \times m_{L}}\right\}, \\ &\Phi_{a}^{ck} = \begin{bmatrix} \Phi_{k} & (0)_{n \times m} & (0)_{n \times m} \\ &\Pi H_{k}^{(c)} & (0)_{m \times m} & (0)_{m \times m} \\ &\Pi H_{k}^{(c)} & (0)_{m \times m} & (0)_{m \times m} \\ &\Pi H_{k}^{(c)} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & \eta_{a}^{\beta i} = \begin{bmatrix} (0)_{n \times n} & (0)_{n \times m} & (0)_{m \times m} \\ & (0)_{m \times n} & (0)_{m \times m} & (0)_{m \times m} \\ & \eta_{a}^{\beta k} = \begin{bmatrix} \Gamma_{k} & (0)_{n \times m} \\ & (0)_{m \times r} & (0)_{m \times m} \\ & (0)_{m \times r} & (0)_{m \times m} \\ & (0)_{m \times r} & (0)_{m \times m} \\ & \eta_{m \times r} & (0)_{m \times m} \\ & \Gamma_{a}^{\xi i} = \begin{bmatrix} (0)_{n \times r} & (0)_{m \times m} \\ & (0)_{m \times r} & (0)_{m \times m} \\ & \eta_{m \times r} & N_{i} \end{bmatrix}, \\ & H_{a}^{ck} = [\Pi H_{k}^{(c)} & (0)_{m \times m} & (0)_{m \times m} \\ & \eta_{m \times r} & N_{i} \end{bmatrix}, \end{split}$$

$$\begin{split} H_a^{\xi_i} &= [N_i H^{(c)} - N_i \Xi - N_i + N_i \Xi], \\ H_a^{\zeta_i} &= [(0)_{m \times n} \ N_i - \Pi N_i \ -N_i + \Pi N_i], \\ H_a^{\gamma_i} &= [(0)_{m \times n} \ -N_i \ N_i], \ i = 1, \cdots, L \\ H_a^{ki} &= [N_i H_k^{(c)} \ (0)_{m \times m} \ (0)_{m \times m}], \\ G_a^{\xi_i} &= [(0)_{m \times r} \ N_i], \ \xi_{iz}(t) = \xi_i(t) - \pi_i, \\ \zeta_{iz}(t) &= \zeta_i(t) - \zeta_i, \ \gamma_{iz}(t) = \xi_{iz}(t)\zeta_{iz}(t). \\ \end{pmatrix} \\ \end{pmatrix}$$

$$\begin{cases} E[\xi_{iz}(t)] = 0, \ E[\xi_{iz}(t)\xi_{jz}^{T}(t)] = 0, \ i \neq j, \\ \sigma_{\xi_{iz}}^{2} = E[\xi_{iz}(t)\xi_{iz}^{T}(t)] = \pi_{i}(1-\pi_{i}), \\ E[\zeta_{iz}(t)] = 0, \ E[\zeta_{iz}(t)\zeta_{jz}^{T}(t)] = 0, \ i \neq j, \\ \sigma_{\zeta_{iz}}^{2} = E[\zeta_{iz}(t)\zeta_{iz}^{T}(t)]\varsigma_{i}(1-\varsigma_{i}), \\ E[\gamma_{iz}(t)] = 0, \ E[\gamma_{iz}(t)\gamma_{jz}^{T}(t)] = 0, \ i \neq j, \\ \sigma_{\gamma_{iz}}^{2} = E[\gamma_{iz}(t)\gamma_{iz}^{T}(t)] = \pi_{i}(1-\pi_{i})\varsigma_{i}(1-\varsigma_{i}). \\ & \overline{\alpha} \, \overline{\beta} \, \overline{\mu} \, \overline{\beta} \xi_{iz}(t), \ \zeta_{iz}(t) \, \overline{\eta} \gamma_{iz}(t) \, \overline{\beta} \, \overline{\eta} \, \overline{\eta} \, \overline{\beta} \, \overline{\mu} \, \overline{\beta} \, \overline{\mu} \, \overline{\beta} \, \overline{\beta$$

声.

注 3 相比于文献 [28–29], 由式(11) 给出的增广状态 *xa*(*t*)具有较小的维数, 如果采用文献 [28–29] 中的方法, 增广 状态的维数为2*n* + 2*m*, 而式(11)给出的增广状态*xa*(*t*)的维 数仅为*n* + 2*m*. 可见, 本文方法可减少计算量.

引理 1^[30] 令 R_i 是 $m_i \times m_i$ 的半正定矩阵,即 $R_i \ge 0$,则块对角矩阵 $R_\delta = \text{diag}\{R_1, \dots, R_L\} \ge 0$.

式(7)中 $v^{(c)}(t)$ 可表示为 $v^{(c)}(t) = D^{(c)}w(t) + \eta^{(c)}(t)$, 且 $D^{(c)} = [D_1^{\mathrm{T}} \cdots D_L^{\mathrm{T}}]^{\mathrm{T}}, \eta^{(c)}(t) = [\eta_1^{\mathrm{T}}(t) \cdots \eta_L^{\mathrm{T}}(t)]^{\mathrm{T}}.$ $\eta^{(c)}(t)$ 的实际和保守方差分别为 $\bar{R}_{\eta_c} = \mathrm{diag}\{\bar{R}_{\eta_1}, \cdots, R_{\eta_L}\}$. 和 $R_{\eta_c} = \mathrm{diag}\{R_{\eta_1}, \cdots, R_{\eta_L}\}$. 用 $R_{\eta_c} \ R_{\eta_c}, \ H$ 应用式(6)和引理1可得: $\bar{R}_{\eta_c} \leq R_{\eta_c}.$ 由式(11)可得 $w_a(t) = F_c w(t) + G_c \eta^{(c)}(t),$ 其中 $F_c = [I_r \ D^{(c)\mathrm{T}}]^{\mathrm{T}},$ $G_c = [(0)_{m \times r} \ I_m]^{\mathrm{T}}.$ 白噪声 $w_a(t)$ 的实际和保守方 差分别为

$$\begin{cases} \bar{Q}_a = F_c \bar{Q} F_c^T + G_c \bar{R}_{\eta_c} G_c^T, \\ Q_a = F_c Q F_c^T + G_c R_{\eta_c} G_c^T. \end{cases}$$
(15)

用 Q_a 减 \bar{Q}_a ,并应用 $\bar{Q} \leq Q$ 和 $\bar{R}_{\eta_c} \leq R_{\eta_c}$ 可得

$$\bar{Q}_a \leqslant Q_a.$$
 (16)

3.2 实际和保守状态二次非中心距

由式(12)可得
$$x_a(t)$$
的保守二次非中心距为
 $X_a(t+1) = \Phi_a^m X_a(t) \Phi_a^{mT} + \sum_{k=1}^{n_\alpha} \sigma_{\alpha_k}^2 \Phi_a^{\alpha k} X_a(t) \Phi_a^{\alpha kT} + \sum_{i=1}^L \sigma_{\xi_{iz}}^2 \Phi_a^{\xi_i} X_a(t) \Phi_a^{\xi_{iT}} + \sum_{i=1}^L \sigma_{\zeta_{iz}}^2 \Phi_a^{\zeta_i} X_a(t) \Phi_a^{\zeta_{iT}} +$

$$\sum_{i=1}^{L} \sigma_{\gamma_{iz}}^{2} \varPhi_{a}^{\gamma_{i}} X_{a}(t) \varPhi_{a}^{\gamma_{i}T} +$$

$$\sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} \varPhi_{a}^{ki} \times X_{a}(t) \varPhi_{a}^{kiT} +$$

$$\Gamma_{a}^{m} Q_{a} \Gamma_{a}^{mT} + \sum_{k=1}^{n_{\beta}} \sigma_{\beta_{k}}^{2} \Gamma_{a}^{\beta_{k}} Q_{a} \Gamma_{a}^{\beta_{k}T} +$$

$$\sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \Gamma_{a}^{\xi_{i}} Q_{a} \Gamma_{a}^{\xi_{i}T}.$$
(17)

带初值 $X_a(0) = \text{diag} \{X(0), (0)_{m \times m}, (0)_{m \times m}\},$ $X(0) = P_0 + \mu_0 \mu_0^{\mathrm{T}}.$ 在式(17)中,分別用 $\bar{X}_a(t), \bar{\sigma}_{\alpha_k}^2,$ $\bar{\sigma}_{\beta_k}^2 和 \bar{Q}_a$ 代替 $X_a(t), \sigma_{\alpha_k}^2, \sigma_{\beta_k}^2 \pi Q_a,$ 可得增广状态 $x_a(t)$ 的实际二次非中心距 $\bar{X}_a(t+1),$ 带初值 $\bar{X}_a(0) =$ $\text{diag} \{\bar{X}(0), (0)_{m \times m}, (0)_{m \times m}\}, \bar{X}(0) = \bar{P}_0 + \mu_0 \mu_0^{\mathrm{T}}.$

引理2 在假设3条件下,可得

$$\bar{X}_a(t) \leqslant X_a(t), \ t \ge 0. \tag{18}$$

证 完全类似于文献[15]中引理5的证明,容易证 得引理2成立. 证毕.

引理3 对于多传感器网络化系统(1)-(4),在 假设1-3条件下,如果 $\rho(\bar{\Phi}_c) < 1, \bar{\Phi}_c = \Phi_a^m \otimes \Phi_a^{mT} + \sum_{k=1}^n \bar{\sigma}_{\alpha_k}^2 \Phi_a^{\alpha k} \otimes \Phi_a^{\alpha k} + \sum_{i=1}^L \sigma_{\xi_{iz}}^2 \Phi_a^{\xi i} \otimes \Phi_a^{\xi i} + \sum_{i=1}^L \sigma_{\zeta_{iz}}^2 \Phi_a^{\zeta i} \otimes \Phi_a^{\zeta i} + \sum_{i=1}^L \sigma_{\gamma_{iz}}^2 \Phi_a^{\gamma i} \otimes \Phi_a^{\gamma i} + \sum_{i=1}^L \sigma_{\xi_{iz}}^2 \sum_{k=1}^{n_\alpha} \bar{\sigma}_{\alpha_k}^2 \Phi_a^{ki} \otimes \Phi_a^{ki},$ 则有如下收敛性:

$$\begin{split} \lim_{t \to \infty} X_a(t) &= X_a, \\ X_a &= \varPhi_a^m X_a \varPhi_a^{m\mathrm{T}} + \sum_{k=1}^{n_a} \sigma_{\alpha_k}^2 \varPhi_a^{\alpha k} X_a \varPhi_a^{\alpha k\mathrm{T}} + \\ &\sum_{i=1}^L \sigma_{\xi_{iz}}^2 \varPhi_a^{\xi_i} X_a \varPhi_a^{\xi_i\mathrm{T}} + \sum_{i=1}^L \sigma_{\zeta_{iz}}^2 \varPhi_a^{\zeta_i} X_a \varPhi_a^{\zeta_i\mathrm{T}} + \\ &\sum_{i=1}^L \sigma_{\gamma_{iz}}^2 \varPhi_a^{\gamma i} X_a \varPhi_a^{\gamma i\mathrm{T}} + \\ &\sum_{i=1}^L \sigma_{\xi_{iz}}^2 \sum_{k=1}^{n_a} \sigma_{\alpha_k}^2 \varPhi_a^{ki} X_a \varPhi_a^{ki\mathrm{T}} + \Gamma_a^m Q_a \Gamma_a^{m\mathrm{T}} + \\ &\sum_{k=1}^{n_\beta} \sigma_{\beta_k}^2 \Gamma_a^{\beta k} Q_a \Gamma_a^{\beta k\mathrm{T}} + \sum_{i=1}^L \sigma_{\xi_{iz}}^2 \Gamma_a^{\xi_i} Q_a \Gamma_a^{\xi_i\mathrm{T}}. \end{split}$$

证 如果 $\rho(\bar{\Phi}_c) < 1$,则类似于文献[24,31]中的 证明过程,通过直接应用文献[32–33]中的结果可证明 引理3成立. 证毕.

在 X_a 的表达式中,分别用 $\bar{X}_a, \bar{\sigma}^2_{\alpha_k}, \bar{\sigma}^2_{\beta_k}$ 和 \bar{Q}_a 代替 $X_a, \sigma^2_{\alpha_k}, \sigma^2_{\beta_k}$ 和 Q_a ,可得实际稳态二次非中心距 \bar{X}_a , 且有收敛性: $\lim_{t\to\infty} \bar{X}_a(t) = \bar{X}_a$. 应用引理3,当 $t \to \infty$ 时,对式(18)取极限可得如下稳态矩阵不等式关系:

$$\bar{X}_a \leqslant X_a. \tag{19}$$

3.3 虚拟过程和观测噪声

增广状态方程(12)可被改写为

$$x_a(t+1) = \Phi_a^m x_a(t) + w_f(t),$$
 (20)

其中 $w_f(t)$ 是虚拟过程噪声,

$$w_{f}(t) = \left(\sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) \varPhi_{a}^{\alpha k} + \sum_{i=1}^{L} \xi_{iz}(t) \varPhi_{a}^{\xi i} + \sum_{i=1}^{L} \zeta_{iz}(t) \varPhi_{a}^{\zeta i} + \sum_{i=1}^{L} \gamma_{iz}(t) \varPhi_{a}^{\gamma i} + \sum_{i=1}^{L} \xi_{iz}(t) \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) \varPhi_{a}^{ki} \right) x_{a}(t) + \left(\Gamma_{a}^{m} + \sum_{k=1}^{n_{\beta}} \beta_{k}(t) \Gamma_{a}^{\beta k} + \sum_{i=1}^{L} \xi_{iz}(t) \Gamma_{a}^{\xi i} \right) w_{a}(t).$$

容易证得 $w_f(t)$ 是零均值白噪声,且它的保守稳态 方差为

$$Q_{f} = \sum_{k1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} \varPhi_{a}^{\alpha k} X_{a} \varPhi_{a}^{\alpha kT} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \varPhi_{a}^{\xi_{i}} X_{a} \varPhi_{a}^{\xi_{i}T} + \sum_{i=1}^{L} \sigma_{\zeta_{iz}}^{2} \varPhi_{a}^{\zeta_{i}} X_{a} \varPhi_{a}^{\zeta_{i}T} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^{2} \varPhi_{a}^{\gamma_{i}} X_{a} \varPhi_{a}^{\gamma_{i}T} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} \varPhi_{a}^{ki} X_{a} \varPhi_{a}^{kiT} + \Gamma_{a}^{m} Q_{a} \Gamma_{a}^{mT} + \sum_{k=1}^{n_{\beta}} \sigma_{\beta_{k}}^{2} \Gamma_{a}^{\beta k} Q_{a} \Gamma_{a}^{\beta kT} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \Gamma_{a}^{\xi_{i}} Q_{a} \Gamma_{a}^{\xi_{i}T}.$$

$$(21)$$

式(21)中分别用 $\bar{X}_a, \bar{\sigma}^2_{\alpha_k}, \bar{\sigma}^2_{\beta_k} \oplus \bar{Q}_a$ 代替 $X_a, \sigma^2_{\alpha_k}, \sigma^2_{\beta_k} \oplus Q_a$,可得 $w_f(t)$ 的实际稳态方差 \bar{Q}_f . 令 $\sigma^2_{\alpha_k} = \bar{\sigma}^2_{\alpha_k} + \Delta \sigma^2_{\alpha_k} \oplus \sigma^2_{\beta_k} = \bar{\sigma}^2_{\beta_k} + \Delta \sigma^2_{\beta_k}, \exists Q_f \bar{M} \bar{Q}_f, \pm \bar{D} \exists$ 式(16)(19),容易证得如下矩阵不等式:

$$\bar{Q}_f \leqslant Q_f. \tag{22}$$

增广集中式融合观测方程(13)可被改写为

$$y^{(c)}(t) = H_a^m x_a(t) + v_f(t),$$
 (23)

其中 $v_f(t)$ 是零均值虚拟观测白噪声, 且 $v_f(t)$ 可表示为

$$v_{f}(t) = \left(\sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) H_{a}^{\alpha k} + \sum_{i=1}^{L} \xi_{iz}(t) H_{a}^{\xi i} + \sum_{i=1}^{L} \zeta_{iz}(t) H_{a}^{\zeta i} + \sum_{i=1}^{L} \gamma_{iz}(t) H_{a}^{\gamma i} + \sum_{i=1}^{L} \xi_{iz}(t) \sum_{k=1}^{n_{\alpha}} \alpha_{k}(t) H_{a}^{ki} \right) x_{a}(t) + \left(G_{a}^{m} + \sum_{i=1}^{L} \xi_{iz}(t) G_{a}^{\xi i} \right) w_{a}(t).$$

它的保守稳态方差为

$$R_f = \sum_{k=1}^{n_\alpha} \sigma_{\alpha_k}^2 H_a^{\alpha k} X_a H_a^{\alpha k \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^2 H_a^{\xi_i} X_a H_a^{\xi_i \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\zeta_{iz}}^2 H_a^{\zeta_i} X_a H_a^{\zeta_i \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^2 H_a^{\gamma_i} X_a H_a^{\gamma_i \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^2 H_a^{\gamma_i} X_a H_a^{\gamma_i} X_a H_a^{\gamma_i} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^2 H_a^{\gamma_i} X_a H_a^{\gamma_i} X_a H_a^{\gamma_i} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^2 H_a^{\gamma_i} X_a H_a^{\gamma_i} + \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^2 H_a^{\gamma_i} X_a H_a^{\gamma_i} + \sum_{i=1}^{L} \sigma_{$$

$$\sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} H_{a}^{ki} X_{a} H_{a}^{ki\mathrm{T}} + G_{a}^{m} Q_{a} G_{a}^{m\mathrm{T}} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} G_{a}^{\xi_{i}} Q_{a} G_{a}^{\xi_{i}\mathrm{T}}.$$
(24)

在式(24)中,分别用 $\bar{X}_{a}, \bar{\sigma}^{2}_{\alpha_{k}} \pi \bar{Q}_{a}$ 代替 $X_{a}, \sigma^{2}_{\alpha_{k}} \pi$ $Q_{a}, 可得v_{f}(t)$ 的实际稳态方差 \bar{R}_{f} .用 R_{f} 减 \bar{R}_{f} ,并应 用式(16)(19),容易证得

$$\bar{R}_f \leqslant R_f. \tag{25}$$

虚拟噪声 $w_f(t)$ 和 $v_f(t)$ 的保守稳态相关矩阵为

$$S_{f} = \sum_{k=1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} \varPhi_{a}^{\alpha k} X_{a} H_{a}^{\alpha k \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \varPhi_{a}^{\xi_{i}} X_{a} H_{a}^{\xi_{i} \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\zeta_{iz}}^{2} \varPhi_{a}^{\zeta_{i}} X_{a} H_{a}^{\gamma_{i} \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\zeta_{iz}}^{2} \varPhi_{a}^{\gamma_{i}} X_{a} H_{a}^{\gamma_{i} \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \sigma_{\alpha_{k}}^{2} \varPhi_{a}^{ki} X_{a} H_{a}^{ki \mathrm{T}} + \Gamma_{a}^{m} Q_{a} G_{a}^{m \mathrm{T}} + \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \Gamma_{a}^{\xi_{i}} Q_{a} G_{a}^{\xi_{i} \mathrm{T}}, \qquad (26)$$

式中分别用 $\bar{X}_{a}, \bar{\sigma}^{2}_{\alpha_{k}}$ 和 \bar{Q}_{a} 代替 $X_{a}, \sigma^{2}_{\alpha_{k}}$ 和 $Q_{a},$ 可得 $w_{f}(t)$ 和 $v_{f}(t)$ 的实际稳态相关矩阵 \bar{S}_{f} .

假设4 假设(Φ_a^m, H_a^m)是完全能检对, ($\bar{\Phi}, \Upsilon$)是 完全能稳对, 其中: $\bar{\Phi} = \Phi_a^m - SH_a^m, S = S_f R_f^{-1},$ $\Upsilon\Upsilon^{\mathrm{T}} = Q_f - S_f R_f^{-1} S_f^{\mathrm{T}}.$

4 鲁棒集中式融合稳态Kalman估值器

4.1 鲁棒集中式融合稳态Kalman预报器

对于由式(20)(23)给出的带已知保守噪声统计 Q_f , $R_f n S_f$ 的最坏情形时不变集中式融合系统,在假设 1-4条件下,基于极大极小鲁棒估计原理^[30],应用标准 Kalman滤波算法^[5],可得保守最优集中式融合稳态一 步Kalman预报器为

$$\hat{x}_{a}^{(c)}(t+1|t) = \Psi^{(c)}\hat{x}_{a}^{(c)}(t|t-1) + K^{(c)}y^{(c)}(t),$$

(27)

$$\Psi^{(c)} = \Phi_a^m - K^{(c)} H_a^m,$$
(28)

$$K^{(c)} = \left(\Phi_a^m P_a^{(c)}(-1) H_a^{mT} + S_f\right) \times (H_a^m P_a^{(c)}(-1) H_a^{mT} + R_f)^{-1}.$$
 (29)

带初值 $\hat{x}_{a}^{(c)}(0|-1) = [\mu_{0}^{T} ((0)_{m \times 1})^{T} ((0)_{m \times 1})^{T}]^{T},$ 且 $\Psi^{(c)}$ 是稳定矩阵.

保守融合稳态一步预报误差方差 $P_a^{(c)}(-1)$ 满足如下稳态Riccati方程:

$$P_{a}^{(c)}(-1) = \Phi_{a}^{m} P_{a}^{(c)}(-1) \Phi_{a}^{mT} - (\Phi_{a}^{m} P_{a}^{(c)}(-1) H_{a}^{mT} + S_{f}) (H_{a}^{m} P_{a}^{(c)}(-1) H_{a}^{mT} + R_{f})^{-1} \times (\Phi_{a}^{m} P_{a}^{(c)}(-1) H_{a}^{mT} + S_{f})^{T} + Q_{f}.$$
 (30)

注 4 由带保守上界 $Q, R_{\eta_i}, \sigma^2_{\alpha_k}, \sigma^2_{\beta_k}$ 和 P_0 的最坏情 形系统(1)-(4)所产生的局部观测 $y_i(t)$ 称为保守局部观测, 它 是不可利用的(未知的). 于是, 由保守局部观测 $y_i(t)$ 组成的 式(8)中给出的保守集中式融合观测 $y^{(c)}(t)$ 也是不可利用的. 由带实际方差 \bar{Q} , \bar{R}_{η_i} , $\bar{\sigma}^2_{\alpha_k}$, $\bar{\sigma}^2_{\beta_k}$ 和 \bar{P}_0 的实际系统(1)-(4)所产 生的局部观测 $y_i(t)$ 称为实际局部观测, 它是通过传感器得到 的, 是可利用的(己知的). 进而, 由实际局部观测 $y_i(t)$ 组成的 式(8)中给出的实际集中式融合观测 $y^{(c)}(t)$ 是可利用的. 在 式(27)中, 用实际融合观测 $y^{(c)}(t)$ 代替保守融合观测 $y^{(c)}(t)$, 可得实际集中式融合Kalman预报器.

定义集中式融合稳态预报误差为 $\tilde{x}_{a}^{(c)}(t+1|t) = x_{a}(t+1) - \hat{x}_{a}^{(c)}(t+1|t),$ 由式(20)减式(27)可得 $\tilde{x}_{a}^{(c)}(t+1|t) = \Psi^{(c)}\tilde{x}_{a}^{(c)}(t|t-1) + w_{f}(t) - K^{(c)}v_{f}(t) = \Psi^{(c)}\tilde{x}_{a}^{(c)}(t|t-1) + [I_{n+2m} - K^{(c)}] \times \lambda_{f}(t),$ (31)

其中: 符号 I_{n+2m} 表示维数为 $(n+2m) \times (n+2m)$ 的 单位矩阵, 增广噪声 $\lambda_f(t) = [w_f^{\mathrm{T}}(t) \ v_f^{\mathrm{T}}(t)]^{\mathrm{T}}$. 容易 得到 $\lambda_f(t)$ 的实际和保守稳态方差分别为

$$\bar{\Lambda}_f = \begin{bmatrix} \bar{Q}_f & \bar{S}_f \\ \bar{S}_f^{\mathrm{T}} & \bar{R}_f \end{bmatrix}, \ \Lambda_f = \begin{bmatrix} Q_f & S_f \\ S_f^{\mathrm{T}} & R_f \end{bmatrix}.$$
(32)

应用式(31)可得保守集中式融合稳态Kalman一步预 报误差方差,也满足如下李雅普诺夫方程:

$$P_{a}^{(c)}(-1) = \Psi^{(c)}P_{a}^{(c)}(-1)\Psi^{(c)T} + [I_{n+2m} - K^{(c)}] \times \Lambda_{f}[I_{n+2m} - K^{(c)}]^{T},$$
(33)

式中分别用 $\bar{P}_{a}^{(c)}(-1)$ 和 $\bar{\Lambda}_{f}$ 代替 $P_{a}^{(c)}(-1)$ 和 Λ_{f} ,可得 实际融合稳态一步预报误差方差 $\bar{P}_{a}^{(c)}(-1)$ 的稳态李 雅普诺夫方程.

引理 4^[30] 令 $\Lambda \ge 0, \Lambda \in \mathbb{R}^{r \times r},$ 设 $\Lambda_{\delta} = (\Lambda_{ij})_{rL \times rL},$ $\Lambda_{ij} = \Lambda, i, j = 1, \cdots, L,$ 则 $\Lambda_{\delta} \ge 0.$

引理5 在假设3条件下,可得如下矩阵不等式 关系: $\bar{\Lambda}_f \leq \Lambda_f$.

证明过程详见附录A.

引理 6^[34] 考虑如下李雅普诺夫方程: $U = CUC^{T} + V$,其中: $U, C \cap V \ge n \times n$ 矩阵, $V \ge N$ 称矩阵, $C \ge R$ 之矩阵(即它的所有特征值都在单位圆内). 如果 $V \ge 0$,则U是对称并唯一的, $\exists U \ge 0$.

定理1 在假设1--4条件下,由式(27)给出的实际集中式融合稳态Kalman预报器具有鲁棒性,即对于所有容许的不确定性,实际预报误差方差 $P_a^{(c)}(-1)$,满足如下关系:

$$\bar{P}_{a}^{(c)}(-1) \leqslant P_{a}^{(c)}(-1),$$
 (34)

且 $P_a^{(c)}(-1)$ 是 $\bar{P}_a^{(c)}(-1)$ 的最小上界.

证明过程详见附录B.

由式(27)给出的实际融合稳态Kalman预报器为鲁

棒融合稳态Kalman预报器,由式(34)给出的矩阵不等 式关系称为它的鲁棒性.

4.2 鲁棒集中式融合稳态Kalman滤波器和平滑器

基于实际集中式融合稳态 Kalman 一步预报器 $\hat{x}_{a}^{(c)}(t|t-1)$,可得实际集中式融合稳态 Kalman 滤波 器(N = 0)和平滑器 $(N > 0)\hat{x}_{a}^{(c)}(t|t+N)$ 为^[35]

$$\hat{x}_{a}^{(c)}(t|t+N) = \hat{x}_{a}^{(c)}(t|t-1) + \sum_{k=0}^{N} K^{(c)}(k) \times \varepsilon^{(c)}(t+k), \ N \ge 0,$$
(35)

$$K^{(c)}(k) = P_a^{(c)}(-1)\Psi^{(c)\text{Tk}}H_a^{m\text{T}}[H_a^m P_a^{(c)}(-1) \times H_a^{m\text{T}} + R_f]^{-1}, \ k \ge 0,$$
(36)

$$\varepsilon^{(c)}(t) = y^{(c)}(t) - H_a^m \hat{x}_a^{(c)}(t|t-1).$$
(37)

类似于文献[35]中的推导,可得集中式融合稳态滤波 和平滑误差 $\tilde{x}_{a}^{(c)}(t|t+N) = x_{a}(t) - \hat{x}_{a}^{(c)}(t|t+N)$ 为

$$\tilde{x}_{a}^{(c)}(t|t+N) = \Psi_{N}^{(c)} \tilde{x}_{a}^{(c)}(t|t-1) + \sum_{\rho=0}^{N} [K_{N\rho}^{cw}, K_{N\rho}^{cv}] \lambda_{f}(t+\rho), \quad (38)$$

利用式(38)可得保守稳态估计误差方差为

$$P_{a}^{(c)}(N) = \Psi_{N}^{(c)} P_{a}^{(c)}(-1) \Psi_{N}^{(c)T} + \sum_{\rho=0}^{N} \left[K_{N\rho}^{cw} \ K_{N\rho}^{cv} \right] \times \Lambda_{f} \left[K_{N\rho}^{cw} \ K_{N\rho}^{cv} \right]^{T}, \ N \ge 0,$$
(39)

式中分别用 $\bar{P}_{a}^{(c)}(N)$, $\bar{P}_{a}^{(c)}(-1)$ 和 $\bar{\Lambda}_{f}$ 代替 $P_{a}^{(c)}(N)$, $P_{a}^{(c)}(-1)$ 和 Λ_{f} ,可得实际估计误差方差 $\bar{P}_{a}^{(c)}(N)$.

定理2 在假设1-4条件下,由式(35)给出的实际集中式融合稳态Kalman滤波器和平滑器具有鲁棒性,即对于所有容许的不确定性,相应的所有实际估计误差方差 $\bar{P}_a^{(c)}(N)$ 满足如下关系:

$$\bar{P}_a^{(c)}(N) \leqslant P_a^{(c)}(N), \ N \ge 0, \tag{40}$$

且 $P_a^{(N)}(-1)$ 是 $\bar{P}_a^{(N)}(-1)$ 的最小上界.

证明过程详见附录C.

由式(35)给出的实际集中式融合稳态Kalman滤波 器和平滑器被称为鲁棒集中式融合稳态Kalman滤波 器和平滑器,由式(40)给出的矩阵不等式关系称为它 们的鲁棒性.

推论1 由 $x_a(t) = [x^{\mathrm{T}}(t) \ z^{(c)^{\mathrm{T}}}(t-1) \ y^{(c)^{\mathrm{T}}}(t-1)]^{\mathrm{T}}$,可得原始系统(1)-(4)的鲁棒集中式融合稳态 Kalman估值器 $\hat{x}^{(c)}(t|t+N) = [I_n \ (0)_{n \times m} \ (0)_{n \times m}]$ $\hat{x}_a^{(c)}(t|t+N), \ N = -1, \ N \ge 0,$ 它们的实际和保守 融合误差方差分别为

$$\bar{P}^{(c)}(N) = \begin{bmatrix} I_n & (0)_{n \times m} & (0)_{n \times m} \end{bmatrix} \bar{P}^{(c)}_a(N) \times \begin{bmatrix} I_n & (0)_{n \times m} & (0)_{n \times m} \end{bmatrix}^{\mathrm{T}},$$
(41)

$$P^{(c)}(N) = [I_n \ (0)_{n \times m} \ (0)_{n \times m}] P_a^{(c)}(N) \times [I_n \ (0)_{n \times m} \ (0)_{n \times m}]^{\mathrm{T}}.$$
 (42)

对所有容许的不确定性,集中式融合稳态Kalman估值 器 $\hat{x}^{(c)}(t|t+N)$ 具有鲁棒性,即

 $\bar{P}^{(c)}(N) \leq P^{(c)}(N), N = -1, N \ge 0,$ (43) 且 $P^{(c)}(N)$ 是 $\bar{P}^{(c)}(N)$ 的最小上界.

推论 2 完全类似于式 (9)–(43) 的推导, 容易得 到原始系统 (1)–(4) 的鲁棒局部稳态 Kalman 估值器 $\hat{x}_i(t|t+N), N = -1, N \ge 0, i = 1, \dots, L$, 且它们 的实际估计误差方差 $\bar{P}_i(N)$ 有相应的最小上界 $P_i(N)$, 即

$$\bar{P}_i(N) \leqslant P_i(N), \ N = -1, \ N \ge 0.$$
(44)

注 5 利用射影理论可以证得

$$P^{(c)}(N) \leqslant P_i(N), \ N = -1, \ N \ge 0, \ i = 1, \dots, L, \quad (45)$$
$$P^{(c)}(N) < P^{(c)}(N-1) < \dots < P^{(c)}(1) <$$
$$P^{(c)}(0) < P^{(c)}(-1), \ N \ge 1. \quad (46)$$

对式(43)-(46)中的矩阵求迹,得到如下矩阵迹不等式关系:

$$\begin{cases} \operatorname{tr} \bar{P}^{(c)}(N) \leqslant \operatorname{tr} P^{(c)}(N), \ \operatorname{tr} \bar{P}_{i}(N) \leqslant \operatorname{tr} P_{i}(N), \\ \operatorname{tr} P^{(c)}(N) \leqslant \operatorname{tr} P_{i}(N), \ N = -1, \ N \ge 0, \ i = 1, \cdots, L, \end{cases}$$
(47)
$$\operatorname{tr} P^{(c)}(N) < \operatorname{tr} P^{(c)}(N-1) < \cdots < \operatorname{tr} P^{(c)}(1) < \\ \operatorname{tr} P^{(c)}(0) < \operatorname{tr} P^{(c)}(-1), \ N \ge 1. \end{cases}$$
(48)

注 6 在注5中, tr $\bar{P}^{(c)}(N)$ 和tr $\bar{P}_i(N)$ 被称为相应鲁棒 Kalman估值器的实际精度, tr $P^{(c)}(N)$ 和tr $P_i(N)$ 被称为鲁棒 精度(或者全局精度). 迹的值越小意味着精度越高. 注5表明, 估值器的实际精度都高于或等于它的鲁棒精度, 鲁棒精度是 最低的实际精度. 集中式融合器的鲁棒精度高于各局部估值 器.

5 带有色观测噪声和混合不确定性的多通 道MA信号估计应用实例

自回归滑动平均(autoregressive MA, ARMA)信号滤波问题经常发生在信号处理、状态估计、目标跟踪、反卷积以及时间序列分析等领域.考虑如下带有色观测噪声和混合不确定性的多传感器多通道MA信

号:

$$s(t) = B_t(q^{-1})u(t),$$
(49)

$$z_i(t) = s(t) + r(t) + \eta_i(t), \ i = 1, \cdots, L,$$
 (50)

$$A_t(q^{-1})r(t) = e(t),$$
(51)

$$y_i(t) = \xi_i(t)z_i(t) + (1 - \xi_i(t))\zeta_i(t)z_i(t - 1) + (1 - \xi_i(t))(1 - \zeta_i(t))y_i(t - 1),$$
(52)

其中:

$$\begin{cases} A_t(q^{-1}) = I_m + A_1(t-1)q^{-1} + \dots + A_p(t-p)q^{-p}, \\ A_k(t) = (a_k^{(gh)}(t))_{m \times m}, \ a_k^{(gh)}(t) = a_k^{(gh)} + \alpha_k^{(gh)}(t), \\ g, h = 1, \dots, m, \ 1 \le k \le p, \end{cases}$$

$$(53)$$

$$\begin{cases} B_t(q^{-1}) = B_1(t-1)q^{-1} + \dots + B_p(t-p)q^{-p}, \\ B_k(t) = (b_k^{(\text{gh})}(t))_{m \times m}, \ b_k^{(\text{gh})}(t) = b_k^{(\text{gh})} + \beta_k^{(\text{gh})}(t), \\ g, h = 1, \dots, m, \ 1 \le k \le p, \end{cases}$$
(54)

其中: $s(t) \in \mathbb{R}^m$ 是被估的多通道信号; $u(t) \in \mathbb{R}^m$ 是 输入噪声; $z_i(t) \in \mathbb{R}^m$ 是第 i^{\uparrow} 传感器收到的观测; $y_i(t) \in \mathbb{R}^m$ 是估值器接收到的观测; $\xi_i(t) \in \mathbb{R}^1$ 和 $\zeta_i(t) \in \mathbb{R}^1, i = 1, \cdots, L$ 是满足式(5)的相互独立的伯 努利白噪声; $r(t) \in \mathbb{R}^m$ 是满足式(51)的有色观测噪 声; $\eta_i(t) \in \mathbb{R}^m$ 是观测白噪声, $e(t) \in \mathbb{R}^m$ 是白噪声. $A_t(q^{-1})$ 和 $B_t(q^{-1})$ 是 q^{-1} 的p阶多项式; q^{-1} 是单位滞 后算子, 即 $q^{-1}s(t) = s(t-1)$; $A_k(t) \in \mathbb{R}^{m \times m}$ 和 $B_k(t) \in \mathbb{R}^m \times m, k = 1, \cdots, p$ 是随机参数矩阵; $a_k^{(\text{gh})}(t)$, $b_k^{(\text{gh})}(t)$ 分别是 $A_k(t)$ 和 $B_k(t)$ 中第g行第h列位置的元 素; $a_k^{(gh)}(t) \in \mathbb{R}^1$ 是带已知均值 $a_k^{(gh)}$ 和随机扰动 $\alpha_k^{(\text{gh})}$ 和随机扰动 $\beta_k^{(\text{gh})}(t)$ 的标量随机元素.

 $u(t), e(t), \eta_i(t), \alpha_k^{(\text{gh})}(t) 和 \beta_k^{(\text{gh})}(t) 是各自不相关 的零均值白噪声, \bar{Q}_u, \bar{Q}_e, \bar{R}_{\eta_i}, \bar{\sigma}_{\alpha_k^{(\text{gh})}}^2 和 \bar{\sigma}_{\beta_k^{(\text{gh})}}^2 分别是 它 们 的 未 知 不 确 定 实 际(真 实)方 差. Q_u, Q_e, R_{\eta_i}, \sigma_{\alpha_k^{(\text{gh})}}^2 和 \sigma_{\beta_k^{(\text{gh})}}^2 分 别 是 \bar{Q}_u, \bar{Q}_e, \bar{R}_{\eta_i}, \bar{\sigma}_{\alpha_k^{(\text{gh})}}^2 \eta \bar{\sigma}_{\beta_k^{(\text{gh})}}^2 \beta \Omega \Omega Q_u, \bar{Q}_e, \bar{Q}_{\eta_i}, \bar{\sigma}_{\beta_k^{(\text{gh})}}^2 \eta \bar{\sigma}_{\beta_k^{(\text$

目的是为多传感器多通道MA信号*s*(*t*)设计鲁棒 集中式融合稳态Kalman估值器.

由式(53)-(54)可得

$$A_k(t) = A_k + \Lambda_k(t), \ B_k(t) = B_k + \Upsilon_k(t), \ 1 \le k \le p.$$
(55)

得

$$1 \leq k \leq p. \Lambda_{k}(t) 和 \Upsilon_{k}(t) 可被改写为$$

$$\begin{cases} \Lambda_{k}(t) = \sum_{g=1}^{m} \sum_{h=1}^{m} \alpha_{k}^{(\mathrm{gh})}(t) \Lambda_{k}^{(\mathrm{gh})}, \\ \Upsilon_{k}(t) = \sum_{g=1}^{m} \sum_{h=1}^{m} \beta_{k}^{(\mathrm{gh})}(t) \Upsilon_{k}^{(\mathrm{gh})}, \end{cases}$$
(56)

其中: $\Lambda_k^{(\text{gh})}$ 和 $\Upsilon_k^{(\text{gh})}$ 都是 $m \times m$ 矩阵, 它们的第g行第 h列元素等于1, 其余元素均为0.

带随机参数矩阵的多通道MA信号模型(49)可被转换为如下等价的状态空间模型^[5]:

$$x_s(t+1) = \Phi_s x_s(t) + \Gamma_s(t)u(t), \qquad (57)$$

$$s(t) = H_s x_s(t), \tag{58}$$

其中:

$$\Phi_{s} = \begin{bmatrix} (0)_{m \times m} & I_{m(p-1)} \\ \vdots & & \\ (0)_{m \times m} & (0)_{m \times m} & \cdots & (0)_{m \times m} \end{bmatrix}, \\
\Gamma_{s}(t) = \begin{bmatrix} B_{1}(t) \\ B_{2}(t) \\ \vdots \\ B_{p}(t) \end{bmatrix}, H_{s} = [I_{m} \ (0)_{m \times m} \ \cdots \ (0)_{m \times m}]$$

将 $B_k(t) = B_k + \Upsilon_k(t)$ 代入 $\Gamma_s(t)$,并应用式(56)得

··· $(0)_{m \times m}$ I_m $(0)_{m \times m}$ ··· $(0)_{m \times m}$]^T, 这里 Γ_{sk} , $k = 1, \cdots, p \not\in mp \times m$ 矩阵, 它的第(k, 1)个块矩阵 为单位矩阵 I_m , 其余位置均为 $(0)_{m \times m}$.

有色观测噪声r(t)有等价的状态空间模型为^[5]

$$x_r(t+1) = \Phi_r(t)x_r(t) + \Gamma_r e(t),$$
 (60)

$$r(t) = H_r(t)x_r(t) + e(t),$$
 (61)

其中:

这里 $\Phi_{rk}, k = 1, \dots, p$ 是 $m \times mp$ 矩阵,它的第(1, k)个块矩阵为单位矩阵 I_m ,其余位置均为 $(0)_{m \times m}$. $H_{rk}, k = 1, \dots, p$ 是 $m \times mp$ 矩阵,它的第(1, k)个块矩阵为 $-I_m$,其余位置均为 $(0)_{m \times m}$.

$$\mathcal{FX}$$

$$x(t) = \begin{bmatrix} x_s(t) \\ x_r(t) \end{bmatrix}, \ \Phi(t) = \begin{bmatrix} \Phi_s & (0)_{mp \times mp} \\ (0)_{mp \times mp} & \Phi_r(t) \end{bmatrix}$$

$$\Gamma(t) = \begin{bmatrix} \Gamma_s(t) & (0)_{mp \times m} \\ (0)_{mp \times m} & \Gamma_r \end{bmatrix}, \ w(t) = \begin{bmatrix} u(t) \\ e(t) \end{bmatrix},$$

$$H(t) = [H_s, \ H_r(t)].$$

于是可得如下增广系统模型:

$$x(t+1) = \Phi(t)x(t) + \Gamma(t)w(t), \tag{63}$$

$$z_i(t) = H(t)x(t) + v_i(t), \ i = 1, \cdots, L,$$
 (64)

$$v_i(t) = e(t) + \eta_i(t),$$
 (65)

其中: 零均值白噪声w(t)的实际和保守方差分别为 $\bar{Q} = \text{diag}\{\bar{Q}_u, \bar{Q}_e\}, Q = \text{diag}\{Q_u, Q_e\}, 用 Q 减去 \bar{Q},$ 并应用引理1可得 $\bar{Q} \leq Q$.

应用式(59)和式(62)可将增广系统(63)-(65)转换 为如下带常参数的系统:

$$x(t+1) = (\Phi + \sum_{k=1}^{p} \sum_{g=1}^{m} \sum_{h=1}^{m} \alpha_{k}^{(\text{gh})}(t) \Phi_{\alpha k}^{(\text{gh})}) x(t) + (\Gamma + \sum_{k=1}^{p} \sum_{g=1}^{m} \sum_{h=1}^{m} \beta_{k}^{(\text{gh})}(t) \Gamma_{\beta k}^{(\text{gh})}) w(t),$$
(66)

$$z_{i}(t) = (H + \sum_{k=1}^{p} \sum_{g=1}^{m} \sum_{h=1}^{m} \alpha_{k}^{(\text{gh})}(t) H_{\alpha k}^{(\text{gh})}) x(t) + v_{i}(t), \ i = 1, \cdots, L,$$
(67)

$$v_i(t) = Dw(t) + \eta_i(t), \tag{68}$$

 $\begin{array}{l} \overset{}{\underset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath{\not H}}{\overset{\scriptstyle \ensuremath{\not H}}}{\overset{\scriptstyle \ensuremath$

因此,应用状态空间方法和增广方法,多通道 MA信号模型(49)-(54)被转换成带乘性噪声、一步随 机观测时滞、丢包和不确定噪声方差的状态空间模型 式(52)(66)-(68).

由式(58)可得 $s(t) = [H_s (0)_{m \times mp}]x(t)$,于是,鲁 棒融合信号估计问题可以通过鲁棒融合状态估计来 解决,应用射影理论^[5]可得

$$\hat{s}^{(c)}(t|t+N) = [H_s \ (0)_{m \times mp}]\hat{x}^{(c)}(t|t+N),$$

$$N = -1, \ N \ge 0.$$
(69)

信号s(t)的实际和保守集中式融合稳态估计误差方差 分别为

$$\begin{cases} \bar{P}^{(c)s}(N) = [H_s \ (0)_{m \times mp}] \bar{P}^{(c)}(N) [H_s \ (0)_{m \times mp}]^{\mathrm{T}}, \\ P^{(c)s}(N) = [H_s \ (0)_{m \times mp}] P^{(c)}(N) [H_s \ (0)_{m \times mp}]^{\mathrm{T}}. \end{cases}$$
(70)

这里, 上角标"s"表示信号.

注 7 对系统(52)(66)–(68),当取m = 1时,MA信号 s(t)是单通道信号,此时系统(52)(66)–(68)可视为系统(1)–(4) 的一种特殊情况,其中: $n_{\alpha}=n_{\beta}=p, \Phi_{k}=\Phi_{\alpha k}^{(11)}, \Gamma_{k}=\Gamma_{\beta k}^{(11)},$ $H_{i}=H, H_{ik}=H_{\alpha k}^{(11)}, D_{i}=D.$

类似式(69)–(70),可得鲁棒局部稳态信号估值器 $\hat{s}_i(t|t+N), N = -1, N \ge 0, i=1, \cdots, L$ 和它的实际和保守局部稳态估计误差方差 $\bar{P}^s_i(N)$ 和 $P^s_i(N)$.容易证得定理1和定理2对信号s(t)成立.

6 仿真实例

在仿真实验中,考虑多传感器单通道MA信号 模型(49)-(54),设m = 1, p = 2, L = 3, $a_1^{(11)} = 0.8$, $a_2^{(11)} = -0.09, b_1^{(11)} = -0.5, b_2^{(11)} = -0.36, \bar{Q}_u = 3$, $Q_u = 4, \bar{Q}_e = 0.05, Q_e = 0.1, \bar{R}_{\eta_1} = 0.25$, $R_{\eta_1} = 0.35, \bar{R}_{\eta_2} = 1, R_{\eta_2} = 1.2, \bar{R}_{\eta_3} = 0.4$, $R_{\eta_3} = 0.6, \bar{\sigma}_{\alpha_1^{(11)}}^2 = 0.01, \sigma_{\alpha_1^{(11)}}^2 = 0.02, \bar{\sigma}_{\alpha_2^{(11)}}^2 = 0.02, \sigma_{\alpha_2^{(11)}}^2 = 0.03, \bar{\sigma}_{\beta_1^{(11)}}^2 = 0.03, \sigma_{\beta_1^{(11)}}^2 = 0.04, \bar{\sigma}_{\beta_2^{(11)}}^2 = 0.04, \sigma_{\beta_2^{(11)}}^2 = 0.05, \pi_1 = 0.9, \pi_2 = \pi_3 = 0.85, \varsigma_1 = 0.85, \varsigma_2 = 0.85, \varsigma_3 = 0.85.$ 仿真结果如下.

由于信号s(t) ∈ R¹, 所以估计误差方差的迹值等 于相应的估计误差方差值. 表1给出了实际和保守局 部与集中式融合稳态估计误差方差的比较, 这验证了 由式(43)-(46)给出的稳态精度关系. 表1中N = -1表示预报器, N = 0表示滤波器, N = 1表示一步平 滑器, N = 2表示两步平滑器.

表1 信号s(t)的稳态鲁棒和实际精度比较

Table 1 Comparison of steady-state robustness and actual accuracy of signal s(t)

	N = -1	N = 0	N = 1	N=2
$P_1^{\mathbf{s}}(N)$	1.7146	0.6788	0.6081	0.5990
$\bar{P}_1^{\mathbf{s}}(N)$	1.2113	0.4412	0.3966	0.3904
$P_2^{\mathbf{s}}(N)$	1.7691	1.0428	0.9655	0.9626
$\bar{P}_2^{\mathrm{s}}(N)$	1.2627	0.7509	0.6978	0.6961
$P_3^{\mathbf{s}}(N)$	1.7456	0.8749	0.7936	0.7884
$\bar{P}_3^{\mathbf{s}}(N)$	1.2360	0.5760	0.5210	0.5171
$P^{(c)s}(N)$	1.6849	0.4886	0.4249	0.4113
$\bar{P}^{(c)s}(N)$	1.1874	0.3099	0.2727	0.2641

图1给出了鲁棒局部和集中式融合稳态一步平滑 器 $\hat{s}_i(t|t+1), i = 1, 2, 3\pi \hat{s}^{(c)}(t|t+1)$ 的跟踪效果. 从图1可看到,鲁棒集中式融合稳态一步平滑器 $\hat{s}^{(c)}(t|t+1)$ 的跟踪性能更好.





图2给出了鲁棒集中式融合稳态信号估值器 $\hat{s}^{(c)}$ (t|t-1), $\hat{s}^{(c)}(t|t)$ 和 $\hat{s}^{(c)}(t|t+1)$ 的跟踪效果. 可看到, 它们的实际估计误差依次减小, 这与式(46)给出的精 度关系一致.

为了说明状态依赖乘性噪声 $\alpha_k^{(11)}(t), k = 1, 2$ 和 噪声依赖乘性噪声 $\beta_k^{(11)}(t), k = 1, 2$ 对鲁棒信号滤 波器 $\hat{s}^{(c)}(t|t)$ 的精度影响, 令 $[\sigma_{\alpha_1^{(11)}}^2 \sigma_{\alpha_2^{(11)}}^2] = \lambda_1[1 \ 1],$ $[\sigma_{\beta_1^{(11)}}^2 \sigma_{\beta_2^{(11)}}^2] = \lambda_2[1 \ 1], \lambda_1 和 \lambda_2$ 按步长0.01从0.01增 加至0.09, 图3给出了鲁棒精度 $P^{(c)s}(0)$ (即tr $P^{(c)s}(0)$) 随着 λ_1 和 λ_2 的增加的变化情况.可看到,当两类噪声 方差增加时, $P^{(c)s}(0)$ 的值也增加,这意味着集中式融 合稳态信号滤波器 $\hat{s}^{(c)}(t|t)$ 的鲁棒精度降低.





Fig. 2 Signal s(t) and its centralized fusion estimator





7 结论

针对在系统状态转移矩阵和观测矩阵中带相同状态依赖乘性噪声,并带噪声依赖乘性噪声、不确定噪声方差、一步随机观测滞后和丢包的多传感器网络化系统,应用增广方法、去随机化方法和虚拟噪声技术将该系统转换为仅带不确定噪声方差的集中式融合系统.转换之后系统的过程噪声和观测噪声是相同的,这可避免求解它们的相关矩阵.根据极大极小鲁棒估计原理,提出了鲁棒集中式融合稳态Kalman估值器(预报器、滤波器和平滑器).应用增广噪声方法、非负定矩阵分解方法和李雅普诺夫方程方法,证明了估值器的鲁棒性.所提出的方法可用于解决带随机参数矩

阵、不确定噪声方差和网络化随机不确定性的多传感 器多通道MA信号的鲁棒融合Kalman滤波问题. 仿真 实验证明了所提出方法的可应用性与正确性.

参考文献:

- LIGGINS M E, HALL D L, LLINAS J. Handbook of Multisensor Data Fusion: Theory and Practice, Second Edition. New York: CRC Press, 2009.
- WANG Z D, NIU Y G. Distributed estimation and filtering for sensor networks. *International Journal of Systems Science*, 2011, 42(9): 1421 1425.
- [3] HU J, WANG Z D, CHEN D Y, et al. Estimation, filtering and fusion for networked systems with network-induced phenomena: Newprogress and prospects. *Information Fusion*, 2016, 31: 65 – 75.
- [4] SUN S L, LIN H L, MA J, et al. Multi-sensor distributed fusion estimation with applications in networked systems: A review paper. *Information Fusion*, 2017, 38: 122 – 134.
- [5] ANDERSON B D O, MOORE J B. Optimal Filtering. NJ: Prentice-Hall, Englewood Cliffs, 1979.
- [6] GAO M, HU J, CHEN D Y, et al. Resilient state estimation for timevarying uncertain dynamical networks with datapacket dropouts and switching topology: Anevent-triggered method. *IET Control Theory* & *Applications*, 2020, 14(3): 367 – 377.
- [7] CHEN B, HU G Q, HO D W C, et al. A new approach to linear/nonlinear distributed fusion estimation problem. *IEEE Transactions on Automatic Control*, 2019, 64(3): 1301 – 1308.
- [8] CHEN B, HU G Q. Nonlinear state estimation under bounded noises. Automatica, 2018, 98: 159 – 168.
- [9] WANG S Y, WANG Z D, DONG H L, et al. Recursive state estimation for linear systems with lossy measurements under timecorrelated multiplicative noises. *Journal of the Franklin Institute*, 2020, 357(3): 1887 – 1908.
- [10] WANG S Y, FANG H J, TIAN X G. Robust estimator design for networked uncertain systems with imperfect measurements and uncertain-covariance noises. *Neurocomputing*, 2017, 230: 40 – 47.
- [11] LIU W, XIE X P, QIAN W, et al. Optimal linear filtering for networked control systems with random matrices, correlated noises, and packet dropouts. *IEEE Access*, 2020, 8: 59987 – 59997.
- [12] LIU W. Optimal estimation for discrete-time linear systems in the presence of multiplicative and time-correlated additive measurement noises. *IEEE Transactions on Signal Processing*, 2015, 63(17): 4583-4593.
- [13] LIU W. Optimal filtering for discrete-time linear systems with timecorrelated multiplicative measurement noises. *IEEE Transactions on Automatic Control*, 2016, 61(7): 1972 – 1978.
- [14] LIU W Q, WANG X M, DENG Z L. Robust centralized and weighted measurement fusion Kalman estimators for uncertain multisensor systems with linearly correlated white noises. *Information Fusion*, 2017, 35: 11 – 25.
- [15] LIU W Q, TAO G L, FAN Y J, et al. Robust fusion steady-state filtering for multisensor networked systems with one-step random delay, missing measurements, and uncertain-variance multiplicative and additive white noises. *International Journal of Robust & Nonlinear Control*, 2019, 29(14): 4716 – 4754.
- [16] LIU W Q, TAO G L, SHEN C. Robust measurement fusion steadystate estimator design for multisensor networked systems with random two-step transmission delays and missing measurements. *Mathematics & Computers in Simulation*, 2021, 181: 242 – 283.
- [17] LIU W Q, DENG Z L. Weighted fusion robust steady-state estimators for multisensor networked systems with one-step random delay and inconsecutive packet dropouts. *International Journal of Adaptive Control & Signal Processing*, 2020, 34(2): 151 – 182.

- [18] LEWIS F L, XIE L H, POPA D. Optimal and Robust Estimation: With an Introduction to Stochastic Control Theory, Second Edition. New York: CRC Press, 2008.
- [19] SUN S L, XIE L H, XIAO W D, et al. Optimal linear estimationfor systems with multiple packet dropouts. *Automatica*, 2008, 44(5): 1333 – 1342.
- [20] MA J, SUN S L. Optimal linear estimators for systems with random sensor delays, multiple packet dropouts and uncertain observations. *IEEE Transactions on Signal Processing*, 2011, 59(11): 5181 – 5192.
- [21] MA J, SUN S L. Centralized fusion estimators for multisensor systems with random sensor delays, multiple packet dropouts and uncertain observations. *IEEE Sensors Journal*, 2013, 13(4): 1228 – 1235.
- [22] WANG S Y, FANG H J, TIAN X G. Minimum variance estimation for linear uncertain systems with one-step correlated noises and incomplete measurements. *Digital Signal Processing*, 2016, 49: 126 – 136.
- [23] LI M Y, ZHANG L, CHU D S. Optimal estimation for systems with multiplicative noises, random delays and multiple packet dropouts. *IET Signal Process*, 2016, 10(8): 880 – 887.
- [24] MA J, SUN S L. Distributed fusion filter for networked stochastic uncertain systems with transmission delays and packet dropouts. *Signal Processing*, 2017, 130: 268 – 278.
- [25] CHEN B, ZHANG W A, HU G Q, et al. Networked fusion Kalman filtering with multiple uncertainties. *IEEE Transactions on Aerospace* & *Electronic Systems*, 2015, 51(3): 2332 – 2349.
- [26] ÁGUILA R C, CARAZO A H, PÉREZ J L. Networked distributed fusion estimation under uncertain outputs with random transmission delays, packet losses and multi-packet processing. *Signal Processing*, 2019, 156: 71 – 83.
- [27] YANG C S, YANG Z B, DENG Z L. Robust weighted state fusion Kalman estimators for networked systems with mixed uncertainties. *Information Fusion*, 2019, 45: 246 – 265.
- [28] RAN C J, DENG Z L. Robust integrated covariance intersection fusion Kalman estimators for networked systems with random measurement delays, multiplicative noises, and uncertain noise variances. *International Journal of Adaptive Control & Signal Processing*, 2020, 34(11): 1697 – 1725.
- [29] RAN C J, DENG Z L. Robust fusion Kalman estimators for networked mixed uncertain systems with random one-step measurement delays, missing measurements, multiplicative noises and uncertain noise variances. *Information Sciences*, 2020, 534: 27 – 52.
- [30] QI W J, ZHANG P, DENG Z L. Robust weighted fusion Kalman filters for multisensor time-varying systems with uncertain noise variances. *Signal Processing*, 2014, 99: 185 – 200.
- [31] LI N, SUN S L, MA J. Multi-sensor distributed fusion filtering for networked systems with different delay and loss rates. *Digital Signal Processing*, 2014, 34: 29 – 38.
- [32] LIU Guangming, SU Weizhou. Survey of linear discrete-time stochastic controls systems with multiplicative noises. *Control Theory & Applications*, 2013, 30(8): 929 946.
 (刘光明,苏为洲. 具有乘性噪声的线性离散时间随机控制系统综述. 控制理论与应用, 2013, 30(8): 929 946.)
- [33] WANG Z D, HO D W C, LIU X H. Robust filtering under randomly varying sensor delay with variance constraints. *Circuits and Systems II: Express Briefs, IEEE Transactions on*, 2004, 51(6): 320 – 326.
- [34] KAILATH T, SAYED A H, HASSIBI B. *Linear Estimation*. NJ: Prentice-Hall, Englewood Cliffs, 2000.
- [35] SUN X J, GAO Y, DENG Z L, et al. Multi-model information fusion Kalman filtering and white noise deconvolution. *Information. Fusion*, 2010, 11(2): 163 – 173.

附录A

证 定义 $\Delta \Lambda_f = \Lambda_f - \bar{\Lambda}_f, \Delta Q_f = Q_f - \bar{Q}_f, \Delta S_f = S_f - \bar{S}_f, \Delta R_f = R_f - \bar{R}_f, \Delta Q_a = Q_a - \bar{Q}_a 和 \Delta X_a = X_a - \bar{X}_a, 且 令 \sigma_{\alpha_k}^2 = \bar{\sigma}_{\alpha_k}^2 + \Delta \sigma_{\alpha_k}^2 \Re \sigma_{\beta_k}^2 = \bar{\sigma}_{\beta_k}^2 + \Delta \sigma_{\beta_k}^2, \oplus$ 式(21),式(24)(26)(32)可得

$$\Delta \Lambda_f = \Delta \Lambda_f^{(1)} + \Delta \Lambda_f^{(2)} + \dots + \Delta \Lambda_f^{(10)} + \Delta \Lambda_f^{(11)},$$

其中:

$$\begin{split} \Delta \Lambda_{f}^{(1)} &= \sum_{k=1}^{n_{\alpha}} \bar{\sigma}_{\alpha_{k}}^{2} M_{a}^{\alpha k} \Delta X_{g} M_{a}^{\alpha k \mathrm{T}}, \\ \Delta \Lambda_{f}^{(2)} &= \sum_{k=1}^{n_{\alpha}} \Delta \sigma_{\alpha_{k}}^{2} M_{a}^{\alpha k} X_{g} M_{a}^{\alpha k \mathrm{T}}, \\ \Delta \Lambda_{f}^{(3)} &= \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} M_{a}^{\xi i} \Delta X_{g} M_{a}^{\xi i \mathrm{T}}, \\ \Delta \Lambda_{f}^{(4)} &= \sum_{i=1}^{L} \sigma_{\zeta_{iz}}^{2} M_{a}^{\zeta i} \Delta X_{g} M_{a}^{\zeta i \mathrm{T}}, \\ \Delta \Lambda_{f}^{(5)} &= \sum_{i=1}^{L} \sigma_{\gamma_{iz}}^{2} M_{a}^{\gamma i} \Delta X_{g} M_{a}^{\gamma i \mathrm{T}}, \\ \Delta \Lambda_{f}^{(6)} &= \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \bar{\sigma}_{\alpha_{k}}^{2} M_{a}^{k i} \Delta X_{g} M_{a}^{k i \mathrm{T}} \\ \Delta \Lambda_{f}^{(6)} &= \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} \sum_{k=1}^{n_{\alpha}} \Delta \sigma_{\alpha_{k}}^{2} M_{a}^{k i} X_{g} M_{a}^{k i \mathrm{T}} \\ \Delta \Lambda_{f}^{(6)} &= \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} N_{a}^{\beta \alpha} \Delta Q_{g} N_{a}^{k i \mathrm{T}}, \\ \Delta \Lambda_{f}^{(9)} &= \sum_{i=1}^{L} \sigma_{\xi_{iz}}^{2} N_{a}^{\beta k} \Delta Q_{g} N_{a}^{\beta k \mathrm{T}}, \\ \Delta \Lambda_{f}^{(10)} &= \sum_{k=1}^{n_{\beta}} \bar{\sigma}_{\beta_{k}}^{2} N_{a}^{\beta k} \Delta Q_{g} N_{a}^{\beta k \mathrm{T}}, \\ \Delta \Lambda_{f}^{(11)} &= \sum_{k=1}^{n_{\beta}} \Delta \sigma_{\beta_{k}}^{2} N_{a}^{\beta k} Q_{g} N_{a}^{\beta k \mathrm{T}}, \end{split}$$

这里:

$$\begin{split} M_a^{\alpha k} &= \operatorname{diag}\{\Phi_a^{\alpha k}, H_a^{\alpha k}\}, \ M_a^{\xi i} &= \operatorname{diag}\{\Phi_a^{\xi i}, H_a^{\xi i}\}, \\ M_a^{\zeta i} &= \operatorname{diag}\{\Phi_a^{\zeta i}, H_a^{\zeta i}\}, \ M_a^{\gamma i} &= \operatorname{diag}\{\Phi_a^{\gamma i}, H_a^{\gamma i}\}, \\ M_a^{k i} &= \operatorname{diag}\{\Phi_a^{k i}, H_a^{k i}\}, \ N_a^m &= \operatorname{diag}\{\Gamma_a^m, G_a^m\}, \\ N_a^{\xi i} &= \operatorname{diag}\{\Gamma_a^{\xi i}, G_a^{\xi i}\}, \ N_a^{\beta k} &= \operatorname{diag}\{\Gamma_a^{\beta k}, 0\}, \\ \Delta X_g &= \begin{bmatrix}\Delta X_a \ \Delta X_a\\ \Delta X_a \ \Delta X_a\end{bmatrix}, \ X_g &= \begin{bmatrix}X_a \ X_a\\ X_a \ X_a\end{bmatrix}, \\ \Delta Q_g &= \begin{bmatrix}\Delta Q_a \ \Delta Q_a\\ \Delta Q_a \ \Delta Q_a\end{bmatrix}, \ Q_g &= \begin{bmatrix}Q_a \ Q_a\\ Q_a \ Q_a\end{bmatrix}. \end{split}$$

由式(19)和引理4得 $\Delta X_g \ge 0$,从而得到 $\Delta \Lambda_f^{(k)} \ge 0, k =$ 1,3,4,5,6. 根据方差矩阵的半正定性,应用引理4可得 $X_g \ge 0$,进而可得 $\Delta \Lambda_f^{(2)} \ge 0, \Delta \Lambda_f^{(7)} \ge 0$.此外,应用式(16) 和引理4可得 $\Delta Q_g \ge 0$,进而可得 $\Delta \Lambda_f^{(k)} \ge 0, k = 8,9,10$. 根据方差矩阵的半正定性,应用引理4可得 $Q_g \ge 0$,进而可 得 $\Delta \Lambda_f^{(11)} \ge 0$.综上可得 $\Delta \Lambda_f = \Delta \Lambda_f^{(1)} + \Delta \Lambda_f^{(2)} + \cdots + \Delta \Lambda_f^{(10)} + \Delta \Lambda_f^{(11)} \ge 0$,即 $\bar{\Lambda}_f \le \Lambda_f$. 证毕.

附录B

证 令
$$\Delta P_a^{(c)}(-1) = P_a^{(c)}(-1) - \bar{P}_a^{(c)}(-1)$$
, 由式(33)得
 $\Delta P_a^{(c)}(-1) = \Psi^{(c)} \Delta P_a^{(c)}(-1) \Psi^{(c)T} + \Delta^{(c)},$

$$\Delta^{(c)} = [I_{n+2m} - K^{(c)}] \Delta \Lambda_f [I_{n+2m} - K^{(c)}]^{\mathrm{T}}.$$

由引理5得 $\Delta^{(c)} \ge 0.$ 由于 $\Psi^{(c)}$ 是稳定矩阵,则由引理6有 $\Delta P_a^{(c)}(-1) \ge 0,$ 即式(34)成立. 取 $\bar{Q} = Q, \bar{R}_{\eta_i} = R_{\eta_i}, \bar{\sigma}_{\alpha_k}^2 = \sigma_{\alpha_k}^2,$ $\bar{\sigma}_{\beta_k}^2 = \sigma_{\beta_k}^2 \pi \bar{P}_0 = P_0, 则假设3仍成立.$ 由 $\bar{R}_{\eta_i} = R_{\eta_i}$ 可得 $\bar{R}_{\eta_c} = R_{\eta_c},$ 于是由式(15)可得 $\bar{Q}_a = Q_a.$ 从 $\bar{X}(0) = \bar{P}_0 + \mu_0 \mu_0^{\mathrm{T}}$ $\pi X(0) = P_0 + \mu_0 \mu_0^{\mathrm{T}}$ 可得 $\bar{X}(0) = X(0),$ 于是有 $\bar{X}_a(0) = X_a(0).$ 通过迭代容易证得 $X_a(t) = \bar{X}_a(t).$ 由引理3可得 $X_a = \bar{X}_a.$ 由式(21)可得 $Q_f = \bar{Q}_f;$ 由式(24)可得 $R_f = \bar{R}_f;$ 由式(26) 可 得 $S_f = \bar{S}_f.$ 由式(32)可得 $\Lambda_f = \bar{\Lambda}_f,$ 于是有 $\Delta^{(c)} = 0.$ 应用引 理6可得 $\Delta P_a^{(c)}(-1) = 0,$ 即 $\bar{P}_a^{(c)}(-1) = P_a^{(c)}(-1).$ 如果 P_a^* 是 $\bar{P}_a^{(c)}(-1)$ 的任意一个其他上界,则有 $P_a^{(c)}(-1) = \bar{P}_a^{(c)}(-1) \leqslant$ $P_a^*,$ 这意味者 $P_a^{(c)}(-1) = \bar{P}_a^{(c)}(-1)$ 的最小上界. 证毕.

附录C

证 令 $\Delta P_a^{(c)}(N) = P_a^{(c)}(N) - \bar{P}_a^{(c)}(N)$, 由式(39)可得

$$\Delta P_{a}^{(c)}(N) = \Psi_{N}^{(c)} \Delta P_{a}^{(c)}(-1) \Psi_{N}^{(c)T} + \sum_{\rho=0}^{N} [K_{N\rho}^{cw} \ K_{N\rho}^{cv}] \times \Delta \Lambda_{f} [K_{N\rho}^{cw} \ K_{N\rho}^{cv}]^{T}.$$

应用引理5和式(34)可得 $\Delta P_a^{(c)}(N) \ge 0$,即式(40)成立. 类似于定理1的证明,可证得 $P_a^{(c)}(N)$ 是 $\bar{P}_a^{(c)}(N)$ 的最小上界, 细节在此省略. 证毕.

作者简介:

陶贵丽博士,讲师,目前研究方向为多传感器信息融合、鲁棒Kalman滤波和广义系统状态估计, E-mail: taoguili_5605@163.com;

李 爽 硕士研究生,目前研究方向为多传感器信息融合和鲁棒 Kalman滤波, E-mail: 1320731630@qq.com;

刘文强 博士,副教授,硕士生导师,目前研究方向为多传感器信息融合、鲁棒Kalman滤波和网络化系统建模,E-mail: lwq@zjgsu.edu. cn.