

具有时变采样周期网络控制系统的严格耗散控制

李媛^{1,2}, 张庆灵^{1†}, 邱占芝³, 蔡敏³

(1. 东北大学 系统科学研究所, 辽宁 沈阳 110819;

2. 沈阳工业大学 理学院, 辽宁 沈阳 110870; 3. 大连交通大学 理学院, 辽宁 大连 116028)

摘要: 研究具有时变采样周期和数据丢包的网络控制系统的渐近稳定和严格耗散控制问题. 针对采样周期时变且在标称周期上下波动, 数据丢包数有界, 利用参数不确定的方法, 网络控制系统建模为一类带有参数不确定的离散时滞系统. 构造一个改进的李雅普诺夫-卡拉索夫斯基函数, 基于线性矩阵不等式方法及 Jensen 不等式方法, 给出系统严格 (Q, S, R) -耗散的充分条件, 得到控制器的设计方法. 数值实例表明所提出的方法具有较小的保守性, 同时也减少了计算量.

关键词: 网络控制系统; 时变采样周期; 数据丢包; 严格耗散控制; 参数不确定性

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Strictly dissipative control for networked control systems with time-varying sampling periods

LI Yuan^{1,2}, ZHANG Qing-ling^{1†}, QIU Zhan-zhi³, CAI Min³

(1. Institute of Systems Science, Northeastern University, Shenyang Liaoning 110819, China;

2. School of Science, Shenyang University of Technology, Shenyang Liaoning 110870, China;

3. School of Science, Dalian Jiaotong University, Dalian Liaoning 116028, China)

Abstract: This paper studies the asymptotic stability and strictly dissipative control problems for networked control systems (NCSs) with time-varying sampling periods and packet dropouts. The sampling period is time-varying and fluctuates across the nominal period. The packet dropouts vary in a bounded interval. The NCSs are modeled as a class of discrete-time system with parametrical uncertainties by the parameter uncertainty method. An improved Lyapunov-Krasovskii function is constructed. On the basis of LMIs formulation and the discrete Jensen inequality, we derive some new sufficient conditions for strict (Q, S, R) -dissipativity, and present the controller design methods. The numerical example shows that the design method is less conservative and with reduced computational complexity in comparison with conventional methods.

Key words: networked control systems (NCSs); time-varying sampling periods; packet dropouts; strictly dissipative control; parameter uncertainty

1 Introduction

Networked control systems (NCSs) are feedback control systems whose feedback paths are implemented by a real-time network. In many modern distributed control systems, remotely located sensors, actuators and controllers are often connected over a shared communication network. Compared with the control system by traditional point to point direct link, there are several advantages for NCSs, for example, less cost of installation, higher flexibility and reliability, easy maintenance and so on^[1-2]. However, communication networks are usually unreliable, and may be subject to undesirable packet dropouts, time-varying sampling periods and network-induced delays, which may significantly degrade the system performance. Therefore, the negative effects caused by communication networks should be taken into account in designing NCSs

to obtain desired control performance.

The interest in the stability of NCSs has grown in recent years due to its theoretical and practical significance^[3-7]. In most of the existing results concerning stability of NCSs, the sampling period is constant. In practical engineering, the actual sampling period often varies due to dynamic bandwidth allocation and scheduling decisions, this variation can degrade the control performance and even make the systems unstable. In [8], the NCS is modeled as a class of discrete time-delay system by the parameter uncertainty method and D -stability of the NCS is studied. But repeated eigenvalues of the coefficient matrix are not considered in [8].

Dissipativeness is an important concept in control theory, and it has been widely applied in stability analysis for linear systems and nonlinear systems. It extends from pas-

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[†]Corresponding author. E-mail: qlzhang@mail.neu.edu.cn; Tel.: +86 024-83689929.

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sitivity analysis and H_∞ performance. The problem of dissipative control has been attracting the attention of many researchers^[9–13]. The dissipativity analysis in discrete-time systems is studied in [9–10]. The robust dissipative control problem for time-delay systems is reported in [11–12]. Robust dissipative control for internet-based switching systems is studied in [13]. But there is virtually no results on strict dissipativity for the NCSs with time-varying sampling periods, which motivates the present dissipativity investigation of the NCSs.

In this paper, the asymptotical stability and strictly dissipative control problems are investigated for the NCSs with time-varying sampling periods and packet dropouts. Sufficient conditions for strict dissipativity are derived via the LMI formulation, and the design of strictly dissipative controller is further given. The paper is organized as follows: In Section 2, the NCSs model with packet dropouts and time-varying sampling periods is made, which is equivalent to a class of discrete time-delay system with parametrical uncertainties by mathematical transformation and matrix theory. The strictly dissipative control problem for the foregoing model is considered in Section 3, and Section 4 is an illustrative example, and Section 5 gives some conclusion remarks.

2 Problem formulation

The structure of the considered NCSs is shown in Fig.1, where the plant is described by the following linear system model:

$$\begin{cases} \dot{x}(t) = A_1x(t) + B_1u(t) + C_1w(t), \\ z(t) = A_2x(t) + B_2u(t) + C_2w(t), \end{cases} \quad (1)$$

where $x(t) \in \mathbb{R}^n$ is the system state vector, $u(t) \in \mathbb{R}^m$ is the control input vector, $w(t) \in \mathbb{R}^p$ is the disturbance input, $z(t) \in \mathbb{R}^q$ is the controlled output, $A_1, A_2, B_1, B_2, C_1, C_2$ are known constant matrices of appropriate dimensions, respectively. Suppose the sensor, the controller and the actuator are clock-driven.

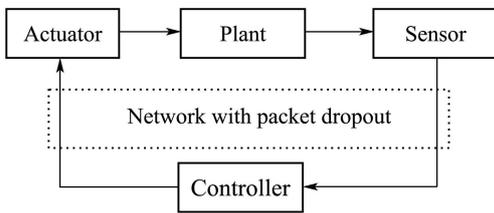


Fig. 1 Diagram of the NCSs with packet dropouts

Assume that T_k is the length of the k th sampling period, t_k is the latest sampling instant, $T_k = t_{k+1} - t_k = \bar{T} + \Delta T_k$ (\bar{T} is the nominal value of the sampling period), and assume that the time-varying sampling interval is bounded, and such that $\Delta T_k = T_k - \bar{T} \in [\Delta T_{\min}, \Delta T_{\max}]$.

Suppose $u(k-L_k)$ ($L_k \geq 1$) is the available control input at the instant t_k , where $L_k - 1$ is the number of consecutive packet dropout, L_{\max} and L_{\min} are the upper-bound and lower-bound of L_k , respectively. So the discrete time expression of the system (1) is as follows:

$$\begin{cases} x(k+1) = \Phi(T_k)x(k) + \Gamma_1(T_k)u(k-L_k) + \Gamma_2(T_k)w(k), \\ z(k) = A_2x(k) + B_2u(k-L_k) + C_2w(k), \end{cases} \quad (2)$$

where

$$\begin{cases} \Phi(T_k) = e^{A_1T_k}, \\ \Gamma_1(T_k) = \int_0^{T_k} e^{A_1t} dt B_1, \\ \Gamma_2(T_k) = \int_0^{T_k} e^{A_1t} dt C_1. \end{cases} \quad (3)$$

Considering the matrix A_1 can be diagonalizable and can be turned into Jordan standard, the NCSs (2) could be modeled as a class of discrete time-delay system with parametrical uncertainties.

1) The matrix A_1 can be diagonalizable.

Let $\lambda_1, \dots, \lambda_n$ be the n different eigenvalues of the matrix A_1 , there exists an invertible matrix Λ , where column vectors of Λ are eigenvectors corresponding to λ_i of A_1 , such that

$$A_1 = \Lambda \text{diag}\{\lambda_1, \dots, \lambda_n\} \Lambda^{-1}. \quad (4)$$

Combining the formula (4), one gets

$$\begin{cases} \Phi(T_k) = \\ \Lambda \text{diag}\{e^{\lambda_1 T_k}, \dots, e^{\lambda_n T_k}\} \Lambda^{-1} = D_1 F_1(T_k) E_1, \\ \Gamma_1(T_k) = \\ \Lambda \text{diag}\{\int_0^{T_k} e^{\lambda_1 t} dt, \dots, \int_0^{T_k} e^{\lambda_n t} dt\} \Lambda^{-1} B_1 = \\ D_{10} + D_{12} F_2(T_k) E_{12}, \\ \Gamma_2(T_k) = \\ \Lambda \text{diag}\{\int_0^{T_k} e^{\lambda_1 t} dt, \dots, \int_0^{T_k} e^{\lambda_n t} dt\} \Lambda^{-1} C_1 = \\ D_{20} + D_{22} F_2(T_k) E_{22}. \end{cases} \quad (5)$$

Where scalars $\alpha_1, \dots, \alpha_n$ meet the following conditions:

① $\lambda_i > 0, \alpha_i > \Delta T_{\max}$; ② $\lambda_i < 0, \alpha_i < \Delta T_{\min}, i = 1, \dots, n$ and

$$\begin{aligned} D_1 &= \Lambda \text{diag}\{e^{\lambda_1(\bar{T}+\alpha_1)}, \dots, e^{\lambda_n(\bar{T}+\alpha_n)}\}, \\ D_{12} &= D_{22} = \\ &\Lambda \text{diag}\left\{\frac{1}{\lambda_1} e^{\lambda_1(\bar{T}+\alpha_1)}, \dots, \frac{1}{\lambda_n} e^{\lambda_n(\bar{T}+\alpha_n)}\right\}, \\ D_{10} &= \Lambda \text{diag}\left\{-\frac{1}{\lambda_1}, \dots, -\frac{1}{\lambda_n}\right\} \Lambda^{-1} B_1, \\ D_{20} &= \Lambda \text{diag}\left\{-\frac{1}{\lambda_1}, \dots, -\frac{1}{\lambda_n}\right\} \Lambda^{-1} C_1, \\ F_1(T_k) &= F_2(T_k) = \\ &\text{diag}\{e^{\lambda_1(\Delta T_k - \alpha_1)}, \dots, e^{\lambda_n(\Delta T_k - \alpha_n)}\}, \\ E_1 &= \Lambda^{-1}, E_{12} = \Lambda^{-1} B_1, E_{22} = \Lambda^{-1} C_1. \end{aligned}$$

2) The matrix A_1 can be turned into Jordan standard.

Let λ^* be the r repeated eigenvalue of the matrix A_1 and the other eigenvalues be different, there exists an invertible matrix Λ , where column vectors of Λ are eigenvectors corresponding to λ_i of A_1 , such that

$$A_1 = \Lambda \text{diag}\{J_1, J_2\} \Lambda^{-1}, \quad (6)$$

where

$$J_1 = \text{diag}\{\lambda_1, \dots, \lambda_{n-r}\},$$

$$J_2 = \begin{bmatrix} 1 & 0 & \cdots & 0 \\ \lambda^* & 1 & \cdots & 0 \\ \vdots & \ddots & \ddots & \vdots \\ \frac{1}{(r-1)!} \lambda^* & \cdots & \lambda^* & 1 \end{bmatrix}.$$

Combining the formula (6), one gets

$$\begin{cases} \Phi(T_k) = \\ \Lambda \text{diag}\{e^{J_1 T_k}, e^{J_2 T_k}\} \Lambda^{-1} = D_1 F_1(T_k) E_1, \\ \Gamma_1(T_k) = \\ \Lambda \int_0^{T_k} \text{diag}\{e^{\lambda_1 t}, \dots, e^{\lambda_{n-r} t}, e^{J_2 t}\} dt \Lambda^{-1} B_1 = \\ D_{10} + D_{12} F_2(T_k) E_{12}, \\ \Gamma_2(T_k) = \\ \Lambda \int_0^{T_k} \text{diag}\{e^{\lambda_1 t}, \dots, e^{\lambda_{n-r} t}, e^{J_2 t}\} dt \Lambda^{-1} C_1 = \\ D_{20} + D_{22} F_2(T_k) E_{22}. \end{cases} \quad (7)$$

Where scalars $\alpha_1, \dots, \alpha_{n-r}$ and matrices M_1, M_2 meet the following conditions: ① $\lambda_i > 0, \alpha_i > \Delta T_{\max}, \lambda_i < 0, \alpha_i < \Delta T_{\min}, i = 1, \dots, n-r$; ② M_1, M_2 are diagonal reversible matrices, $\|M_1^{-1} \hat{J}_2\| < 1, \|M_2^{-1} \check{J}_2\| < 1$, and

$$\begin{aligned} D_1 &= \Lambda \text{diag}\{e^{\lambda_1(\bar{T} + \alpha_1)}, \dots, D_{n-r}, M_1\}, \\ D_{12} &= D_{22} = \\ &\Lambda \text{diag}\left\{\frac{1}{\lambda_1} e^{\lambda_1(\bar{T} + \alpha_1)}, \dots, \frac{1}{\lambda_{n-r}} D_{n-r}, M_2\right\}, \\ D_{10} &= \Lambda \text{diag}\left\{-\frac{1}{\lambda_1}, \dots, -\frac{1}{\lambda_{n-r}}, \check{J}_2\right\} \Lambda^{-1} B_1, \\ D_{20} &= \Lambda \text{diag}\left\{-\frac{1}{\lambda_1}, \dots, -\frac{1}{\lambda_{n-r}}, \check{J}_2\right\} \Lambda^{-1} C_1, \\ F_1(T_k) &= \text{diag}\{e^{\lambda_1(\Delta T_k - \alpha_1)}, \dots, F_{n-r}, M_1^{-1} \hat{J}_2\}, \\ F_2(T_k) &= \text{diag}\{e^{\lambda_1(\Delta T_k - \alpha_1)}, \dots, F_{n-r}, M_2^{-1} \check{J}_2\}, \\ E_1 &= \Lambda^{-1}, E_{12} = \Lambda^{-1} B_1, E_{22} = \Lambda^{-1} C_1, \\ \hat{J}_2 &= \begin{bmatrix} e^{\lambda^* T_k} & 0 & \cdots & 0 \\ T_k e^{\lambda^* T_k} & e^{\lambda^* T_k} & \cdots & 0 \\ \vdots & \ddots & \ddots & \vdots \\ \frac{(T_k)^{r-1}}{(r-1)!} e^{\lambda^* T_k} & \cdots & T_k e^{\lambda^* T_k} & e^{\lambda^* T_k} \end{bmatrix}, \\ \check{J}_2 &= \begin{bmatrix} -\frac{1}{\lambda^*} & 1 & \cdots & 1 \\ \frac{1}{(\lambda^*)^2} & -\frac{1}{\lambda^*} & \cdots & 1 \\ \vdots & \ddots & \ddots & \vdots \\ (-1)^r \frac{1}{(\lambda^*)^r} & \cdots & \frac{1}{(\lambda^*)^2} & -\frac{1}{\lambda^*} \end{bmatrix}, \\ \tilde{J}_2 &= \begin{bmatrix} \frac{1}{\lambda^*} e^{\lambda^* T_k} & 0 & \cdots & 0 \\ \tilde{J}_{22} & \frac{1}{\lambda^*} e^{\lambda^* T_k} & \cdots & 0 \\ \vdots & \ddots & \ddots & \vdots \\ \tilde{J}_{2r} & \cdots & \tilde{J}_{22} & \frac{1}{\lambda^*} e^{\lambda^* T_k} \end{bmatrix}, \end{aligned}$$

$$\begin{aligned} \tilde{J}_{22} &= \frac{1}{(\lambda^*)^2} (\lambda^* T_k - 1) e^{\lambda^* T_k}, \\ \tilde{J}_{2r} &= \frac{1}{(\lambda^*)^r} \sum_{j=1}^r \frac{(-1)^{j+1} (\lambda^* T_k)^{r-j}}{(r-j)!} e^{\lambda^* T_k}, \\ D_{n-r} &= e^{\lambda_{n-r}(\bar{T} + \alpha_{n-r})}, \\ F_{n-r} &= e^{\lambda_{n-r}(\Delta T_k - \alpha_{n-r})}. \end{aligned}$$

Definition 1 The quadratic energy supply function E associated with the system (2) is defined by

$$E(w, z, T) = \langle z, Qz \rangle_T + 2\langle z, Sw \rangle_T + \langle w, R w \rangle_T, \quad (8)$$

where Q, S, R are real matrices of appropriate dimensions with Q, R symmetric.

Definition 2^[13-15] The system (2) with energy supply E is said to be (Q, S, R) -dissipative, if for any $T \geq 0$ and some real function $\eta(\cdot)$ with $\eta(0) = 0$,

$$E(w, z, T) + \eta(x_0) \geq 0.$$

Furthermore, if for any scalar $\alpha > 0$,

$$E(w, z, T) + \eta(x_0) \geq \alpha \langle w, w \rangle_T, \quad (9)$$

the system (2) is said to be strictly (Q, S, R) -dissipative.

Remark 1 The above performance of strict (Q, S, R) -dissipativity includes H_∞ performance and passivity as special cases:

1) When $Q = -I, S = 0$ and $R = \gamma^2 I$, (9) reduces to a H_∞ norm constraint^[16-17].

2) When $Q = 0, S = I$ and $R = 0$, (9) reduces to a strict passive problem^[18-19].

Without loss of generality, we make the following assumption.

Assumption 1 1) $Q \leq 0$; 2) $R + C_2^T S + S^T C_2 + C_2^T Q C_2 > 0$.

A static controller is considered here with the form

$$u(k) = Kx(k), \quad (10)$$

where K is the controller gain to be determined. Substituting the formula (10) into (2) and combining (5)-(7), we can obtain the following closed-loop system:

$$\begin{cases} x(k+1) = \tilde{A}_1 x(k) + \tilde{B}_1 x(k-L_k) + \tilde{C}_1 w(k), \\ z(k) = A_2 x(k) + \tilde{B}_2 x(k-L_k) + C_2 w(k), \end{cases} \quad (11)$$

where

$$\begin{aligned} \tilde{A}_1 &= D_1 F_1(T_k) E_1, \\ \tilde{B}_1 &= (D_{10} + D_{12} F_2(T_k) E_{12}) K, \\ \tilde{C}_1 &= D_{20} + D_{22} F_2(T_k) E_{22}, \tilde{B}_2 = B_2 K. \end{aligned}$$

The following lemmas will be used in this paper.

Lemma 1^[20] For any positive semi-definite symmetric matrix $W \in \mathbb{R}^{n \times n}$, if the two positive integers r and r_0 satisfy $r \geq r_0 \geq 1$, the following inequality holds:

$$\begin{aligned} & \left(\sum_{i=r_0}^r x(i) \right)^T W \left(\sum_{i=r_0}^r x(i) \right) \leq \\ & (r - r_0 + 1) \sum_{i=r_0}^r x^T(i) W x(i). \end{aligned}$$

Lemma 2^[21] Let $\Sigma_1, \Sigma_2, \Sigma_3, \Sigma$ with $\Sigma = \Sigma^T > 0$ be real constant matrices with appropriate dimensions and $\Delta(k)$ be a real matrix function satisfying $\Delta^T(k)\Delta(k) \leq I$, then for any scalar $\rho > 0$, the following matrix inequality holds:

$$(\Sigma_3 + \Sigma_1 \Delta(k) \Sigma_2) \Sigma^{-1} (\Sigma_3 + \Sigma_1 \Delta(k) \Sigma_2)^{-1} \leq \rho^{-1} \Sigma_1 \Sigma_1^T + \rho \Sigma_3 (\Sigma - \rho \Sigma_2^T \Sigma_2)^{-1} \Sigma_3^T.$$

Lemma 3^[22] For any matrices $U \in \mathbb{R}^{n \times n}$ and $V \in \mathbb{R}^{n \times n}$, if the matrix V satisfies $V > 0$, then we have

$$V^{-1} \geq U + U^T - U^T V U.$$

The purpose of this paper is to design a state-feedback stabilizing controller (10) such that the resulting closed-loop system (11) is asymptotically stable and strictly (Q, S, R) -dissipative. Then, the strictly dissipative control problem for the NCSs addressed in this paper is expressed as follows.

3 Main results

Theorem 1 For given scalars $L_{\max} > 0, L_{\min} > 0$ and matrices Q, S, R with Q, R symmetric, the system (11) is asymptotically stable and strictly (Q, S, R) -dissipative, if there exist symmetric positive-definite matrices $P, W, Q_1, Q_2, Z_1, Z_2, Z_3$ satisfying the following matrix inequality

$$\begin{bmatrix} A_1 & A_2 \\ A_2^T & A_3 \end{bmatrix} < 0, \tag{12}$$

where

$$\left\{ \begin{aligned} & A_1 = \begin{bmatrix} A_{11} & 0 & Z_1 & Z_2 & -A_2^T S & (Q_-^{\frac{1}{2}} A_2)^T \\ * & A_{22} & Z_3 & Z_3 & -\tilde{B}_2^T S & (Q_-^{\frac{1}{2}} \tilde{B}_2)^T \\ * & * & A_{33} & 0 & 0 & 0 \\ * & * & * & A_{44} & 0 & 0 \\ * & * & * & * & A_{55} & (Q_-^{\frac{1}{2}} C_2)^T \\ * & * & * & * & * & -I \end{bmatrix}, \\ & A_{11} = -P + (\tilde{L} + 1)W + Q_1 + Q_2 - Z_1 - Z_2, \\ & A_{22} = -W - 2Z_3, \\ & A_{33} = -Q_1 - Z_1 - Z_3, \\ & A_{44} = -Q_2 - Z_2 - Z_3, \\ & \tilde{L} = L_{\max} - L_{\min}, \\ & A_{55} = -C_2^T S - S^T C_2 - (R - \alpha I), \\ & A_2^T = \begin{bmatrix} \tilde{A}_1 & \tilde{B}_1 & 0 & 0 & \tilde{C}_1 & 0 \\ L_{\min}(\tilde{A}_1 - I) & L_{\min} \tilde{B}_1 & 0 & 0 & L_{\min} \tilde{C}_1 & 0 \\ \tilde{L}(\tilde{A}_1 - I) & \tilde{L} \tilde{B}_1 & 0 & 0 & \tilde{L} \tilde{C}_1 & 0 \\ L_{\max}(\tilde{A}_1 - I) & L_{\max} \tilde{B}_1 & 0 & 0 & L_{\max} \tilde{C}_1 & 0 \end{bmatrix}, \\ & A_3 = \text{diag}\{-P^{-1}, -Z_1^{-1}, -Z_2^{-1}, -Z_3^{-1}\}. \end{aligned} \right. \tag{13}$$

Proof Construct the following Lyapunov-Krasovskii function:

$$\left\{ \begin{aligned} & V(k) = V_1(k) + V_2(k) + V_3(k) + V_4(k) + V_5(k), \\ & V_1(k) = x^T(k) P x(k), \\ & V_2(k) = \sum_{l=k-L_k}^{k-1} x^T(l) W x(l), \\ & V_3(k) = \sum_{l=k-L_{\min}}^{k-1} x^T(l) Q_1 x(l) + \sum_{l=k-L_{\max}}^{k-1} x^T(l) Q_2 x(l), \\ & V_4(k) = \sum_{l=-L_{\max}+1}^{-L_{\min}} \sum_{j=k+l}^{k-1} x^T(j) W x(j), \\ & V_5(k) = L_{\min} \sum_{l=-L_{\min}}^{-1} \sum_{j=k+l}^{k-1} y^T(j) Z_1 y(j) + L_{\max} \sum_{l=-L_{\max}}^{-1} \sum_{j=k+l}^{k-1} y^T(j) Z_2 y(j) + \tilde{L} \sum_{l=-L_{\max}}^{-L_{\min}-1} \sum_{j=k+l}^{k-1} y^T(j) Z_3 y(j), \end{aligned} \right. \tag{14}$$

where $y(j) = x(j+1) - x(j)$. So

$$\begin{aligned} \Delta V_1(k) &= (\tilde{A}_1 x(k) + \tilde{B}_1 x(k-L_k) + \tilde{C}_1 w(k))^T P (\tilde{A}_1 x(k) + \tilde{B}_1 x(k-L_k) + \tilde{C}_1 w(k)) - x^T(k) P x(k), \end{aligned} \tag{15}$$

$$\begin{aligned} \Delta V_2(k) &= x^T(k) W x(k) - x^T(k-L_k) W x(k-L_k) + \sum_{l=k+1-L_{\min}}^{k-1} x^T(l) W x(l) - \sum_{l=k+1-L_k}^{k-1} x^T(l) W x(l) + \sum_{l=k+1-L_{k+1}}^{k-L_{\min}} x^T(l) W x(l), \end{aligned} \tag{16}$$

$$\begin{aligned} \Delta V_3(k) &= x^T(k) Q_1 x(k) - x^T(k-L_{\min}) Q_1 x(k-L_{\min}) + x^T(k) Q_2 x(k) - x^T(k-L_{\max}) Q_2 x(k-L_{\max}), \end{aligned} \tag{17}$$

$$\begin{aligned} \Delta V_4(k) &= \tilde{L} x^T(k) W x(k) - \sum_{l=k+1-L_{\max}}^{k-L_{\min}} x^T(l) W x(l), \end{aligned} \tag{18}$$

$$\begin{aligned} \Delta V_5(k) &= L_{\min}^2 y^T(k) Z_1 y(k) - L_{\min} \sum_{l=k-L_{\min}}^{k-1} y^T(l) Z_1 y(l) + L_{\max}^2 y^T(k) Z_2 y(k) - L_{\max} \sum_{l=k-L_{\max}}^{k-1} y^T(l) Z_2 y(l) + \tilde{L}^2 y^T(k) Z_3 y(k) - \tilde{L} \sum_{l=k-L_{\max}}^{k-L_{\min}-1} y^T(l) Z_3 y(l). \end{aligned} \tag{19}$$

To notice that $L_k \geq L_{\min}, L_{k+1} \leq L_{\max}$, so

$$\begin{aligned} \Delta V_2(k) &\leq x^T(k) W x(k) - x^T(k-L_k) W x(k-L_k) + \sum_{l=k+1-L_{\max}}^{k-L_{\min}} x^T(l) W x(l). \end{aligned} \tag{20}$$

Using Lemma 1, we have that

$$\begin{aligned}
 & -L_{\min} \sum_{l=k-L_{\min}}^{k-1} y^T(l) Z_1 y(l) \leq \\
 & -\left(\sum_{l=k-L_{\min}}^{k-1} y(l)\right)^T Z_1 \left(\sum_{l=k-L_{\min}}^{k-1} y(l)\right) = \\
 & -(x(k) - x(k - L_{\min}))^T Z_1 (x(k) - \\
 & x(k - L_{\min})), \tag{21}
 \end{aligned}$$

$$\begin{aligned}
 & -L_{\max} \sum_{l=k-L_{\max}}^{k-1} y^T(l) Z_2 y(l) \leq \\
 & -\left(\sum_{l=k-L_{\max}}^{k-1} y(l)\right)^T Z_2 \left(\sum_{l=k-L_{\max}}^{k-1} y(l)\right) = \\
 & -(x(k) - x(k - L_{\max}))^T Z_2 (x(k) - \\
 & x(k - L_{\max})), \tag{22}
 \end{aligned}$$

$$\begin{aligned}
 & -\tilde{L} \sum_{l=k-L_{\max}}^{k-L_{\min}-1} y^T(l) Z_3 y(l) = \\
 & -\tilde{L} \sum_{l=k-L_{\max}}^{k-L_k-1} y^T(l) Z_3 y(l) - \\
 & \tilde{L} \sum_{l=k-L_k}^{k-L_{\min}-1} y^T(l) Z_3 y(l) \leq \\
 & -\left(\sum_{l=k-L_{\max}}^{k-L_k-1} y(l)\right)^T Z_3 \left(\sum_{l=k-L_{\max}}^{k-L_k-1} y(l)\right) - \\
 & \left(\sum_{l=k-L_k}^{k-L_{\min}-1} y(l)\right)^T Z_3 \left(\sum_{l=k-L_k}^{k-L_{\min}-1} y(l)\right) = \\
 & -(x(k - L_k) - x(k - L_{\max}))^T Z_3 (x(k - \\
 & L_k) - x(k - L_{\max})) - (x(k - L_{\min}) - x(k - \\
 & L_k))^T Z_3 (x(k - L_{\min}) - x(k - L_k)). \tag{23}
 \end{aligned}$$

Combining (15)–(23), we have that when $w(k) = 0$,

$$\begin{aligned}
 \Delta V(k) & \leq \\
 & x^T(k+1) P x(k+1) + x^T(k) ((\tilde{L} + 1)W + \\
 & Q_1 + Q_2 - P)x(k) - x^T(k - L_k) W x(k - L_k) + \\
 & (x(k+1) - x(k))^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \\
 & \tilde{L}^2 Z_3) (x(k+1) - x(k)) - x^T(k - L_{\min}) \cdot \\
 & Q_1 x(k - L_{\min}) - x^T(k - L_{\max}) Q_2 x(k - L_{\max}) - \\
 & (x(k) - x(k - L_{\min}))^T Z_1 (x(k) - x(k - L_{\min})) - \\
 & (x(k) - x(k - L_{\max}))^T Z_2 (x(k) - x(k - L_{\max})) - \\
 & (x(k - L_k) - x(k - L_{\max}))^T Z_3 (x(k - L_k) - \\
 & x(k - L_{\max})) - (x(k - L_{\min}) - x(k - L_k))^T \cdot \\
 & Z_3 (x(k - L_{\min}) - x(k - L_k)) = \xi^T(k) \Phi' \xi(k), \tag{24}
 \end{aligned}$$

where

$$\xi(k) = \begin{bmatrix} x(k) \\ x(k - L_k) \\ x(k - L_{\min}) \\ x(k - L_{\max}) \end{bmatrix}, \quad \Phi' = \begin{bmatrix} \Phi'_{11} & \Phi'_{12} & Z_1 & Z_2 \\ \star & \Phi'_{22} & Z_3 & Z_3 \\ \star & \star & \Phi'_{33} & 0 \\ \star & \star & \star & \Phi'_{44} \end{bmatrix},$$

$$\begin{aligned}
 \Phi'_{11} & = \tilde{A}_1^T P \tilde{A}_1 - P + (\tilde{L} + 1)W + Q_1 + Q_2 - \\
 & Z_1 - Z_2 + (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \\
 & \tilde{L}^2 Z_3) (\tilde{A}_1 - I), \\
 \Phi'_{12} & = (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \\
 & \tilde{L}^2 Z_3) \tilde{B}_1 + \tilde{A}_1^T P \tilde{B}_1,
 \end{aligned}$$

$$\begin{aligned}
 \Phi'_{15} & = (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \\
 & \tilde{L}^2 Z_3) \tilde{C}_1 + \tilde{A}_1^T P \tilde{C}_1 - A_2^T Q C_2 - A_2^T S, \\
 \Phi'_{22} & = \tilde{B}_1^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{B}_1 + \\
 & \tilde{B}_1^T P \tilde{B}_1 - W - 2Z_3 - \tilde{B}_2^T Q \tilde{B}_2, \\
 \Phi'_{25} & = \tilde{B}_1^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{C}_1 + \\
 & \tilde{B}_1^T P \tilde{C}_1 - \tilde{B}_2^T Q C_2 - \tilde{B}_2^T S, \\
 \Phi'_{33} & = -Q_1 - Z_1 - Z_3, \quad \Phi'_{44} = -Q_2 - Z_2 - Z_3, \\
 \Phi'_{55} & = \tilde{C}_1^T (P + L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{C}_1 - \\
 & C_2^T Q C_2 - C_2^T S - S^T C_2 - (R - \alpha I).
 \end{aligned}$$

$$\begin{aligned}
 \Phi'_{22} & = \tilde{B}_1^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{B}_1 + \\
 & \tilde{B}_1^T P \tilde{B}_1 - W - 2Z_3, \\
 \Phi'_{33} & = -Q_1 - Z_1 - Z_3, \quad \Phi'_{44} = -Q_2 - Z_2 - Z_3.
 \end{aligned}$$

By Schur complement and (24), if (12) holds, we have that

$$\begin{aligned}
 \Delta V(k) & \leq -\lambda_{\min}(-\Phi') \xi^T(k) \xi(k) \leq \\
 & -\alpha \xi^T(k) \xi(k) \leq -\alpha x^T(k) x(k), \tag{25}
 \end{aligned}$$

where $\alpha = \inf\{\lambda_{\min}(-\Phi')\}$. This proves that the system (11) is asymptotically stable for $L_{\min} \leq L_k \leq L_{\max}$.

Combining (12) and (24), one gets

$$\begin{aligned}
 \Delta V(k) & - z^T(k) Q z(k) - 2z^T(k) S w(k) - \\
 & w^T(k) (R - \alpha I) w(k) \leq \\
 & [\xi^T(k) \quad w^T(k)] \tilde{\Phi}' [\xi^T(k) \quad w^T(k)]^T \leq 0, \tag{26}
 \end{aligned}$$

where

$$\tilde{\Phi}' = \begin{bmatrix} \tilde{\Phi}'_{11} & \tilde{\Phi}'_{12} & Z_1 & Z_2 & \tilde{\Phi}'_{15} \\ \star & \tilde{\Phi}'_{22} & Z_3 & Z_3 & \tilde{\Phi}'_{25} \\ \star & \star & \Phi'_{33} & 0 & 0 \\ \star & \star & \star & \Phi'_{44} & 0 \\ \star & \star & \star & \star & \tilde{\Phi}'_{55} \end{bmatrix},$$

$$\begin{aligned}
 \tilde{\Phi}'_{11} & = \tilde{A}_1^T P \tilde{A}_1 - P + (\tilde{L} + 1)W + Q_1 + Q_2 - \\
 & Z_1 - Z_2 + (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \\
 & \tilde{L}^2 Z_3) (\tilde{A}_1 - I) - A_2^T Q A_2, \\
 \tilde{\Phi}'_{12} & = (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{B}_1 + \\
 & \tilde{A}_1^T P \tilde{B}_1 - \tilde{A}_2^T Q \tilde{B}_2, \\
 \tilde{\Phi}'_{15} & = (\tilde{A}_1 - I)^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{C}_1 + \\
 & \tilde{A}_1^T P \tilde{C}_1 - A_2^T Q C_2 - A_2^T S, \\
 \tilde{\Phi}'_{22} & = \tilde{B}_1^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{B}_1 + \\
 & \tilde{B}_1^T P \tilde{B}_1 - W - 2Z_3 - \tilde{B}_2^T Q \tilde{B}_2, \\
 \tilde{\Phi}'_{25} & = \tilde{B}_1^T (L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{C}_1 + \\
 & \tilde{B}_1^T P \tilde{C}_1 - \tilde{B}_2^T Q C_2 - \tilde{B}_2^T S, \\
 \tilde{\Phi}'_{33} & = -Q_1 - Z_1 - Z_3, \quad \tilde{\Phi}'_{44} = -Q_2 - Z_2 - Z_3, \\
 \tilde{\Phi}'_{55} & = \tilde{C}_1^T (P + L_{\min}^2 Z_1 + L_{\max}^2 Z_2 + \tilde{L}^2 Z_3) \tilde{C}_1 - \\
 & C_2^T Q C_2 - C_2^T S - S^T C_2 - (R - \alpha I).
 \end{aligned}$$

Taking (26) the sum from 0 to T , since $V(x(T+1)) \geq 0$, we have that

$$\begin{aligned}
 E(w, z, T) & = \\
 & \langle z, Qz \rangle_T + 2\langle z, Sw \rangle_T + \langle w, R w \rangle_T \geq \\
 & \alpha \langle w, w \rangle_T + \sum_{k=0}^T [V(k+1) - V(k)] = \\
 & \alpha \langle w, w \rangle_T + V(T+1) - V(0) \geq \\
 & \alpha \langle w, w \rangle_T - V(0).
 \end{aligned}$$

Therefore, from the Definition 2, we can get the system (11) is strictly (Q, S, R) -dissipative. This completes the proof.

Remark 2 In this paper, it is in contrast with [13] for an improved Lyapunov-Krasovskii functional, the added term

$\tilde{L} \sum_{l=-L_{\max}}^{-L_{\min}-1} \sum_{j=k+l}^{k-1} y^T(j)Z_3y(j)$ of the Lyapunov-Krasovskii functional in this paper can reduce conservative. Another differential method to deal with the cross term problem by using the discrete Jensen inequality, neither system transformation nor free-weighting matrix is required, which decreases calculational amount.

Theorem 2 For given scalars $L_{\max} > 0, L_{\min} > 0, \rho > 0$ and matrices Q, S, R with Q, R symmetric, the system (11) is asymptotically stable and strictly (Q, S, R) -dissipative, if there exist symmetric positive-definite matrices $X, \tilde{W}, \tilde{Q}_1, \tilde{Q}_2, \tilde{Z}_1, \tilde{Z}_2, \tilde{Z}_3$ and matrix Y satisfying the following LMI:

$$\begin{bmatrix} \tilde{\Lambda}_1 & \sqrt{\rho} \tilde{\Sigma}_3 & \tilde{\Sigma}_1 & 0 \\ * & \tilde{\Lambda}_3 & 0 & \rho \Sigma_2^T \\ * & * & -\rho I & 0 \\ * & * & * & -\rho I \end{bmatrix} < 0, \quad (27)$$

where

$$\left\{ \begin{aligned} & \tilde{\Lambda}_1 = \begin{bmatrix} \tilde{\Lambda}_{11} & 0 & \tilde{Z}_1 & \tilde{Z}_2 & -(A_2X)^T S & (Q^{\frac{1}{2}} A_2X)^T \\ * & \tilde{\Lambda}_{22} & \tilde{Z}_3 & \tilde{Z}_3 & -(B_2Y)^T S & (Q^{\frac{1}{2}} B_2Y)^T \\ * & * & \tilde{\Lambda}_{33} & 0 & 0 & 0 \\ * & * & * & \tilde{\Lambda}_{44} & 0 & 0 \\ * & * & * & * & \tilde{\Lambda}_{55} & (Q^{\frac{1}{2}} C_2)^T \\ * & * & * & * & * & -I \end{bmatrix}, \\ & \tilde{\Lambda}_{11} = -X + (\tilde{L} + 1)\tilde{W} + \tilde{Q}_1 + \tilde{Q}_2 - \tilde{Z}_1 - \tilde{Z}_2, \\ & \tilde{\Lambda}_{22} = -\tilde{W} - 2\tilde{Z}_3, \tilde{\Lambda}_{33} = -\tilde{Q}_1 - \tilde{Z}_1 - \tilde{Z}_3, \\ & \tilde{\Lambda}_{44} = -\tilde{Q}_2 - \tilde{Z}_2 - \tilde{Z}_3, \tilde{L} = L_{\max} - L_{\min}, \\ & \tilde{\Lambda}_{55} = -C_2^T S - S^T C_2 - (R - \alpha I), \\ & \tilde{\Lambda}_3 = \text{diag}\{-X, -X - X^T + \tilde{Z}_1, \\ & \quad -X - X^T + \tilde{Z}_2, -X - X^T + \tilde{Z}_3\}, \\ & \tilde{\Sigma}_1 = \begin{bmatrix} E_1 X & 0 & 0 & 0 & 0 & 0 \\ 0 & E_{12} Y & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & E_{22} & 0 \end{bmatrix}^T, \\ & \Sigma_2^T = \begin{bmatrix} D_{11}^T & L_{\min} D_{11}^T & \tilde{L} D_{11}^T & L_{\max} D_{11}^T \\ D_{12}^T & L_{\min} D_{12}^T & \tilde{L} D_{12}^T & L_{\max} D_{12}^T \\ D_{22}^T & L_{\min} D_{22}^T & \tilde{L} D_{22}^T & L_{\max} D_{22}^T \end{bmatrix}, \\ & \tilde{\Sigma}_3^T = \begin{bmatrix} 0 & D_{10} Y & 0 & 0 & D_{20}^T & 0 \\ -L_{\min} X & L_{\min}(D_{10} Y) & 0 & 0 & L_{\min} D_{20} & 0 \\ -\tilde{L} X & \tilde{L}(D_{10} Y) & 0 & 0 & \tilde{L} D_{20} & 0 \\ -L_{\max} X & L_{\max}(D_{10} Y) & 0 & 0 & L_{\max} D_{20} & 0 \end{bmatrix}. \end{aligned} \right. \quad (28)$$

Furthermore, the desired controller gain is given by $K = YX^{-1}$.

Proof Replacing $\tilde{\Lambda}_1, \tilde{\Sigma}_1$ and $\tilde{\Sigma}_2$ in (12) with $D_1 F_1(T_k) E_1, (D_{10} + D_{12} F_2(T_k) E_{12}) K, D_{20} + D_{22} F_2(T_k) E_{22}$ and $B_2 K$, respectively, we find that (12) is equivalent to the following inequality:

$$(\Sigma_3 + \Sigma_1 \Delta(T_k) \Sigma_2) (-\Lambda_3)^{-1} (\Sigma_3 + \Sigma_1 \Delta(T_k) \Sigma_2)^T + \Lambda_1 < 0, \quad (29)$$

where

$$\Sigma_1 = \begin{bmatrix} E_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & E_{12} K & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & E_{22} & 0 \end{bmatrix}^T,$$

$$\Sigma_3 = \begin{bmatrix} 0 & -L_{\min} I & -\tilde{L} I & -L_{\max} I \\ (D_{10} K)^T & \Sigma_{31} & \Sigma_{32} & \Sigma_{33} \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ D_{20}^T & L_{\min} D_{20}^T & \tilde{L} D_{20}^T & L_{\max} D_{20}^T \\ 0 & 0 & 0 & 0 \end{bmatrix},$$

$$\Sigma_{31} = L_{\min}(D_{10} K)^T, \Sigma_{32} = \tilde{L}(D_{10} K)^T,$$

$$\Sigma_{33} = L_{\max}(D_{10} K)^T,$$

$$\Delta(T_k) = \text{diag}\{F_1^T(T_k), F_2^T(T_k), F_2^T(T_k)\}.$$

Since $F_1^T(T_k)F_1(T_k) < I, F_2^T(T_k)F_2(T_k) < I$, we have $\Delta^T(T_k)\Delta(T_k) < I$. For any scalar $\rho > 0$, using Lemma 2 and Schur complement, if the following inequality is feasible, (29) is also feasible.

$$\Lambda_1 + \rho^{-1} \Sigma_1 \Sigma_1^T + \rho \Sigma_3 (-\Lambda_3 - \rho \Sigma_2^T \Sigma_2)^{-1} \Sigma_3^T < 0. \quad (30)$$

Using Schur complement again, if the following inequality holds, the inequality (30) holds.

$$\begin{bmatrix} \Lambda_1 & \sqrt{\rho} \Sigma_3 & \Sigma_1 & 0 \\ * & \Lambda_3 & 0 & \rho \Sigma_2^T \\ * & * & -\rho I & 0 \\ * & * & * & -\rho I \end{bmatrix} < 0. \quad (31)$$

Let

$$T = \text{diag}\{T_1, T_2, T_3, T_2\},$$

$$T_1 = \text{diag}\{X, X, X, X, I, I\},$$

$$T_2 = \text{diag}\{I, I, I, I\}, T_3 = \text{diag}\{I, I, I, I, I, I\}.$$

Pre- and post- multiply (31) by T^T and T , and define

$$P^{-1} = X, X^T W X = \tilde{W}, X^T Q_1 X = \tilde{Q}_1,$$

$$X^T Q_2 X = \tilde{Q}_2, X^T Z_1 X = \tilde{Z}_1, X^T Z_2 X = \tilde{Z}_2,$$

$$X^T Z_3 X = \tilde{Z}_3, K X = Y,$$

we can obtain

$$\begin{bmatrix} \tilde{\Lambda}_1 & \sqrt{\rho} \tilde{\Sigma}_3 & \tilde{\Sigma}_1 & 0 \\ * & \Lambda_3 & 0 & \rho \Sigma_2^T \\ * & * & -\rho I & 0 \\ * & * & * & -\rho I \end{bmatrix} < 0. \quad (32)$$

By Lemma 3, we can get

$$\begin{cases} -Z_1^{-1} \leq -X - X^T + X^T Z_1 X, \\ -Z_2^{-1} \leq -X - X^T + X^T Z_2 X, \\ -Z_3^{-1} \leq -X - X^T + X^T Z_3 X. \end{cases} \quad (33)$$

According to the inequalities (33), if (27) is feasible, (32) is also feasible. The proof is completed.

In order to illustrate the generality of our analysis and synthesis approach, we offer the following results.

Corollary 1 For given scalars $L_{\max} > 0, L_{\min} > 0, \rho > 0$, the system (11) is asymptotically stable with disturbance attenuation γ , if there exist symmetric positive-definite matrices $X, \tilde{W}, \tilde{Q}_1, \tilde{Q}_2, \tilde{Z}_1, \tilde{Z}_2, \tilde{Z}_3$ and matrix satisfying the following LMI:

$$\begin{bmatrix} \tilde{\Lambda}_1 & \sqrt{\rho} \tilde{\Sigma}_3 & \tilde{\Sigma}_1 & 0 \\ \star & \tilde{\Lambda}_3 & 0 & \rho \Sigma_2^T \\ \star & \star & -\rho I & 0 \\ \star & \star & \star & -\rho I \end{bmatrix} < 0, \quad (34)$$

where

$$\tilde{\Lambda}_1 = \begin{bmatrix} \tilde{\Lambda}_{11} & 0 & \tilde{Z}_1 & \tilde{Z}_2 & 0 & (A_2 X)^T \\ \star & \tilde{\Lambda}_{22} & \tilde{Z}_3 & \tilde{Z}_3 & 0 & (B_2 Y)^T \\ \star & \star & \tilde{\Lambda}_{33} & 0 & 0 & 0 \\ \star & \star & \star & \tilde{\Lambda}_{44} & 0 & 0 \\ \star & \star & \star & \star & -\gamma^2 I & C_2^T \\ \star & \star & \star & \star & \star & -I \end{bmatrix}. \quad (35)$$

Furthermore, the desired controller gain is given by $K = YX^{-1}$.

Corollary 2 For given scalars $L_{\max} > 0, L_{\min} > 0, \rho > 0$, the system (11) is asymptotically stable and strictly positive, if there exist symmetric positive-definite matrices $X, \tilde{W}, \tilde{Q}_1, \tilde{Q}_2, \tilde{Z}_1, \tilde{Z}_2, \tilde{Z}_3$ and matrix Y satisfying the following LMI:

$$\begin{bmatrix} \tilde{\Lambda}_1 & \sqrt{\rho} \tilde{\Sigma}_3 & \tilde{\Sigma}_1 & 0 \\ \star & \tilde{\Lambda}_3 & 0 & \rho \Sigma_2^T \\ \star & \star & -\rho I & 0 \\ \star & \star & \star & -\rho I \end{bmatrix} < 0, \quad (36)$$

where

$$\tilde{\Lambda}_1 = \begin{bmatrix} \tilde{\Lambda}_{11} & 0 & \tilde{Z}_1 & \tilde{Z}_2 & -(A_2 X)^T & 0 \\ \star & \tilde{\Lambda}_{22} & \tilde{Z}_3 & \tilde{Z}_3 & -(B_2 Y)^T & 0 \\ \star & \star & \tilde{\Lambda}_{33} & 0 & 0 & 0 \\ \star & \star & \star & \tilde{\Lambda}_{44} & 0 & 0 \\ \star & \star & \star & \star & -C_2^T - C_2 & 0 \\ \star & \star & \star & \star & \star & -I \end{bmatrix}. \quad (37)$$

Furthermore, the desired controller gain is given by $K = YX^{-1}$.

Remark 3 According to Theorem 2, Corollary 1 can be deduced by setting $Q = -I, S = 0, (R - \alpha I) = \gamma^2 I$. Corollary 2 can be deduced by setting $Q = 0, S = I, (R - \alpha I) = 0$.

4 Numerical example

Considering an unstable system as follows

$$\begin{cases} \dot{x}(t) = \begin{bmatrix} -0.36 & -1.12 \\ -0.40 & 1.11 \end{bmatrix} x(t) + \begin{bmatrix} 0.41 \\ -1.22 \end{bmatrix} u(t) + \begin{bmatrix} 1.31 \\ 0.62 \end{bmatrix} w(t), \\ z(t) = [-0.31 \quad -0.02]x(t) - 0.68u(t) + 0.32w(t). \end{cases} \quad (38)$$

Suppose $\bar{T} = 0.4$ s, $\Delta T_{\max} = 0.06$ s, $\Delta T_{\min} = -0.02$ s, we discretize the system (38) and can obtain

$$E_1 = \begin{bmatrix} 0.7887 & -0.7734 \\ 0.3651 & 1.0425 \end{bmatrix}, E_{12} = \begin{bmatrix} 1.2669 \\ -1.1222 \end{bmatrix},$$

$$E_{22} = \begin{bmatrix} 0.5537 \\ 1.1246 \end{bmatrix}, D_1 = \begin{bmatrix} 0.9585 & 0.4016 \\ -0.3357 & 0.4096 \end{bmatrix},$$

$$D_{10} = \begin{bmatrix} -37.6343 \\ 12.4628 \end{bmatrix}, D_{20} = \begin{bmatrix} -15.6963 \\ 6.2149 \end{bmatrix},$$

$$D_{12} = D_{22} = \begin{bmatrix} 29.7498 & -0.2673 \\ -10.4183 & -0.2726 \end{bmatrix},$$

$$F_1(T_k) = F_2(T_k) = \text{diag}\{e^{\lambda_1(\Delta T_k - \alpha_1)}, e^{\lambda_2(\Delta T_k - \alpha_2)}\}.$$

where $\lambda_1 = 0.0322, \lambda_2 = -1.5022, \alpha_1 = 0.08, \alpha_2 = -0.03$, then $F_1(T_k), F_2(T_k)$ satisfy $F_1^T(T_k)F_1(T_k) \leq I, F_2^T(T_k)F_2(T_k) \leq I$.

For simplicity, suppose $L_{\max} = 3, L_{\min} = 1$. Applying Theorem 2, we obtain the stabilizing networked controller gain $K = [-0.0309 \quad -0.0059]$. To simulate, we take the initial state as $x(0) = [1 \quad -1]^T$, the system state response and controlled output with above parameters can be seen in Fig.2.

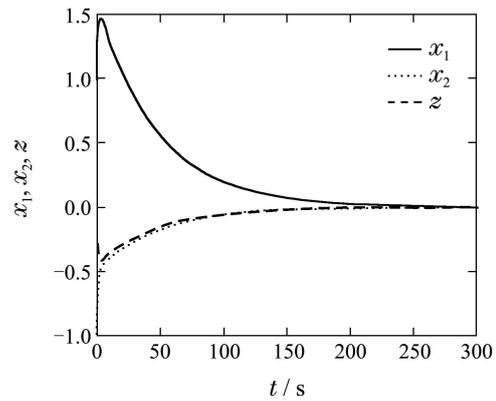


Fig. 2 State response and controlled output of the NCSs

5 Conclusions

The asymptotic stability and strictly dissipative control problems for the NCSs with packet dropouts and time-varying sampling periods have been discussed in this paper. The time-varying sampling period fluctuates across the nominal period. The number of packet dropouts is assumed to have both an upper-bound and a lower-bound. An improved Lyapunov-Krasovskii functional has been constructed. The discrete Jensen inequality is used to deal with the cross term. Based on the LMIs formulation, some new sufficient conditions for strict (Q, S, R) -dissipativity have been derived, and the controller design methods have been presented. A numerical example has illustrated the effectiveness of the proposed approach.

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作者简介:

李媛 (1974–), 女, 副教授, 博士研究生, 目前研究方向为网络控制、鲁棒控制、随机系统等, E-mail: syliyy@163.com;

张庆灵 (1956–), 男, 教授, 博士生导师, 目前研究方向为广义大系统的鲁棒控制、网络控制等, E-mail: qlzhang@mail.neu.edu.cn;

邱占芝 (1960–), 女, 教授, 博士生导师, 目前研究方向为计算机远程监控、网络控制等, E-mail: zhanzhiquok@163.com;

蔡敏 (1964–), 男, 教授, 目前研究方向为无线通信信号处理、功率控制、网络控制的等, E-mail: dlcaim@126.com.